

UNCLASSIFIED

AD NUMBER
AD915628
NEW LIMITATION CHANGE
TO Approved for public release, distribution unlimited
FROM Distribution authorized to U.S. Gov't. agencies only; Test and Evaluation; NOV 1973. Other requests shall be referred to Commander, Army Armament Research and Development Center, Attn: SMCAR-MSI. Dover, NJ 07801.
AUTHORITY
ARDEC ltr, 26 Jan 2010

THIS PAGE IS UNCLASSIFIED

AD 915628



COPY NO. 36

TECHNICAL REPORT 4588

SPIN-73
AN UPDATED VERSION OF THE SPINNER
COMPUTER PROGRAM

ROBERT H. WHYTE

NOVEMBER 1973

Distribution limited to U. S. Government agencies only (test and evaluation; November 1973). Other requests for this document must be referred to Picatinny Arsenal, Dover, New Jersey, ATTN: SARPA-TS-T-S.

PICATINNY ARSENAL

DOVER, NEW JERSEY

07801

The findings in this report are not to be construed
as an official Department of the Army position.

DISPOSITION

Destroy this report when no longer needed. Do not
return to the originator.

Technical Report 4588

SPIN-73
AN UPDATED VERSION OF THE SPINNER
COMPUTER PROGRAM

by

Robert H. Whyte

November 1973

AMCMS Code No. 554C.12.62000

Distribution limited to U.S. Government agencies only (test and evaluation; November 1973). Other requests for this document must be referred to Picatinny Arsenal, Dover, New Jersey, ATTN: SARPA-TS-T-S.

Conducted for

Feltman Research Laboratory
Picatinny Arsenal
Dover, New Jersey 07801

under

Contract No. DAAA21-73-C-0033

by

Armament Systems Department
General Electric Co.
Burlington, VT 05401

FOREWORD

This report documents tasks accomplished by the Armament Systems Department, General Electric Company, Burlington, Vermont under United States Government Contract No. DAAA21-73-C-0033 during the period from 14 August 1972 to 14 July 1973.

ACKNOWLEDGEMENT

The author wishes to acknowledge the personnel of the Free Flight Branch of the Ballistic Research Laboratories, Aberdeen Proving Grounds; the Aeroballistic Branch of Picatinny Arsenal; and the Aeroballistics Branch (Range G) Arnold Engineering Development Center for their cooperation in the collection and interpretation of data used in this study.

ABSTRACT

The SPINNER computer program has been updated to compute aerodynamic coefficients for a wide variety of spin stabilized projectile shapes. Improvements over the original program are substantial as ogive radius, meplat diameter and rotating band diameter are accounted for instead of assuming mean values. Test cases are shown comparing the 1969 SPINNER, the 1973 SPINNER and experimental data. Input instructions and sample program outputs are given along with the 1973 program listing.

TABLE OF CONTENTS

	<u>Page</u>
Foreword	1
Acknowledgement	2
Abstract	3
List of Tables	5
List of Figures	6
Nomenclature	7
Introduction	9
Procedure	11
Empirical Equations	13
Results and Discussion	19
Conclusions and Recommendations	21
References	22
 Appendix A Curve Fit Technique	 71
Appendix B Input - Output - Description	75
Appendix C Program Listing SPIN-73	78
 Distribution List.	 87

LIST OF TABLES

		<u>Page</u>
1	Coefficient Probable Errors	28
2	SPIN-73 Output 20MM M56A3	29
3	SPIN-73 Output 20MM 5 CAL ANSR	32
4	SPIN-73 Output 20MM 7 CAL ANSR	35
5	SPIN-73 Output 20MM 9 CAL ANSR	38
6	SPIN-73 Output 20MM 10 CAL CONE CYL.	41
7	SPIN-73 Output 90MM M71	44
8	SPIN-73 Output 105MM M1	47
9	SPIN-73 Output 105MM XM380E5	50
10	SPIN-73 Output 5/38 NAVY	53
11	SPIN-73 Output 5/54 NAVY	56
12	SPIN-73 Output 155MM M101/107	59
13	SPIN-73 Output 155MM M549	62
14	SPIN-73 Output 175MM M437	65
15	SPIN-73 Output 175MM SRC	68

LIST OF FIGURES

		<u>Page</u>
1	Projectile Parameter Model	27
2	Aerodynamic Data 20MM M56A3	30
3	Aerodynamic Data 20MM 5 CAL. ANSR	33
4	Aerodynamic Data 20MM 7 CAL. ANSR	36
5	Aerodynamic Data 20MM 9 CAL. ANSR	39
6	Aerodynamic Data 20MM 10 CAL. CONE CYL.	42
7	Aerodynamic Data 90MM M71	45
8	Aerodynamic Data 105MM M1	48
9	Aerodynamic Data 105MM XM380E5	51
10	Aerodynamic Data 5/38 NAVY	54
11	Aerodynamic Data 5/54 NAVY	57
12	Aerodynamic Data 155M M101/107	60
13	Aerodynamic Data 155MM M549	63
14	Aerodynamic Data 175MM M437	66
15	Aerodynamic Data 175MM SRC	69

NOMENCLATURE

A	projectile cross-sectional area, ft ²
C _{lp}	spin deceleration coefficient, $M_{lp}/\bar{q}Ad(\frac{pd}{2V})$
C _m	pitching moment coefficient, $M_m/\bar{q}Ad$
C _{m_q}	damping moment coefficient, $M_{mq}/\bar{q}Ad(qd/2V)$
C _{n_p}	magnus moment coefficient, $M_{np}/\bar{q}Ad(pd/2V)$
C _N	normal force coefficient, $F_N/\bar{q}A$
C _{Yp}	magnus force coefficient, $F_{Yp}/\bar{q}A(pd/2V)$
C _X	axial force coefficient, $F_X/\bar{q}A$
CG	center of gravity, calibers from nose
I _x	axial moment of inertia, slug-ft ²
I _y	transverse moment of inertia, slug-ft ²
F _N	normal force, lbs.
F _{Yp}	magnus force, lbs.
F _X	axial force, lbs.
M _{lp}	spin damping moment
M _m	pitching moment about CG
M _{m_q}	damping moment about CG
M _{n_p}	magnus moment about CG
V	total velocity, ft/sec.
d	projectile diameter, ft.
g	gravity, 32.174 ft/sec ²
m	projectile mass, slugs
p	projectile spin rate, radians/second
q	projectile pitch rate, radians/second

NOMENCLATURE (Continued)

\bar{q}	dynamic pressure, $1/2\rho v^2$, lb/ft ²
$\bar{\alpha}$	total angle of attack, radians
ρ	air density, slugs/ft ³

Subscripts

α	Derivative with respect to $\sin \bar{\alpha}$
2	Derivative with respect to $\sin^2 \bar{\alpha}$
α_3	Derivative with respect to $\sin^3 \bar{\alpha}$
α_5	Derivative with respect to $\sin^5 \bar{\alpha}$

INTRODUCTION

The Armament Department of General Electric under contract to Picatinny Arsenal has developed an empirical computerized model for predicting the aerodynamic coefficients of spin stabilized projectiles. The code name of the new program is SPIN-73.

The starting point for the current study was the computer program SPINNFR^{70*} which was developed at Picatinny Arsenal during the period from September 1966 to October 1968. This program was modified by General Electric in 1969⁶⁸ and 1970⁷¹ to update the predictions of the drag coefficient and also to perform a closed form dispersion analysis.

In general the method used during the development of the original Spinner was as follows:

Basic projectile configurations were selected which were considered by Whyte^{68,70} to have well determined aerodynamic coefficients. Empirical equations and constants were developed, by a trial and error process, by which the standard coefficients could be adjusted for changes in total length, nose length, boattail length and center of gravity.

The following limitations were and are present in the original program.

1. Nose length 1.8 to 4.0 calibers
2. Projectile length 3.6 to 9.0 calibers
3. Boattail length 0.0 to 1.0 calibers
4. Meplot diameter, 0.10 to 0.15 calibers
5. Nose radius, secant +100% to secant -30%
6. Rotating band diameter, 1.025 calibers

* References alphabetically listed starting on page 22.

However as most projectiles in service and under investigation during the period from 1966 to 1969 in general fell within the above bounds the limitations of the program were not considered very serious.

Since 1970 several programs have been initiated by the Army and Navy which are considering utilizing projectiles with nose lengths of up to 5.5 calibers and boattail lengths of up to 2.5 calibers.

Also payload and fuzing capabilities of several small arms projectiles currently under development by the Air Force, Navy, and Army have dictated blunter ogives (large meplats) and near tangent ogives.

Rotating band diameter are also of larger scale on small arms than corresponding shapes of large calibers thereby complicating the prediction process.

Because of these known limitations and future requirements the need for a revised SPINNER was indicated. Thus this current study was initiated in August 1972.

Sears⁶⁰ of Eglin in 1972 published a computerized curve fit technique for predicting the drag of projectile. His results indicated improvement over the original SPINNER in the area of tangent ogives and meplat bluntness.

A similar method to that used by Sears was employed in updating SPINNER. In discussing the computer programs the 1969 version of SPINNER will be referred to as SPIN-69 and the 1973 version as SPIN-73.

PROCEDURE

The most difficult task in the analysis of data is determining a constant accurate model which will adequately curve fit data under all circumstances, whereupon predictions of results under a different sets of initial conditions do not result in completely useless answers.

An example of useless results is shown in figure 15 where the predicted axial force is negative in the SPIN-69 program. When terms of higher order polynomials are employed to obtain good fits one must be very cautious when using these polynomials to extrapolate or even interpolate data. These cautions are pointed out because SPIN-73 does employ higher order polynomials.

The equations used for fitting and probable errors will be covered for each coefficient individually.

In general the data utilized with very few exceptions was obtained from reports published by the Ballistic Research Laboratory (BRL) and Arnold Engineering Development Center (AEDC). No wind tunnel data was used at all in the data bank. Wind tunnel data was used to determine trends and comparisons were made with the trends resulting data fitting.

The references utilized to collect the experimental data are listed starting on page 22. Unpublished data from BRL, Picatinny, AEDC and GE were also used. The method used to curve fit the data is described briefly in Appendix A.

Equations of the following general form were used for all coefficients. Definitions of VL, VN, VB, VCG, BD, DM, OR, and BOOM are found in figure 1.

$$\begin{aligned}
C_X = & a_1 + a_2 (CVN) + a_3 (CVN^2) \\
& + a_3 (CXCL) + a_4 (CXCL^2) \\
& + a_5 (CVN \cdot CXCL) \\
& + a_6 (CVB) + a_7 (CBD) \\
& + a_8 (CMK) + a_9 (CMK^2) \\
& + a_{10} (CVN \cdot CMK) + a_{11} (CXCL \cdot CMK) \\
& + a_{11} (CRAT) + \dots \text{ etc.}
\end{aligned}$$

where:

$$CVN = VN - 2.5$$

$$CXCL = VL - VN - VB - 1.5$$

$$CVB = VB$$

$$CBD = BD - 1.02$$

$$CMK = CMK - 1.05$$

$$CRAT = VN^2/OR - 0.40$$

The combinations, variations, and parameters which can be included in the fitting equation are nearly infinite. References such as Dickenson,¹⁹⁻²⁸ Sears,⁶⁰ Watt,⁶⁶ and Murphy⁴³ were used as guides for determining the most effective way of deriving an empirical equation. By the trial and error process equations of the above type were manipulated into a form which adequately described the experimental data.

EMPIRICAL EQUATIONS

This section will describe individually for each coefficient the equations contained in the computer program SPIN-73 as of June 1973.

Axial Force Coefficient

$$CXCL = VL - VN - VB - 1.5$$

$$CBD = DB - 1.02$$

$$CDM = (DM - 0.12)^2 \quad CRAT = VN^2/OR - 0.40$$

$$\text{if } 0 < VN < 3.0 \quad \text{set } VNX = VN, \quad DXN = 0.0$$

$$\text{if } 0 < CXCL < 1.5 \quad \text{set } CXCLL = CXCL, \quad DXCL = 0.0$$

$$\text{if } 0.2 < VB < 0.65 \quad \text{set } VBX = VB - 0.2 \quad DXBT = 0.0$$

If VN, CXCL, or VB are greater than the maximum

$$\text{set } VNX = 3.0, \quad DXN = (VN - 3.0) A_{13}$$

$$CXCLL = 1.5, \quad DXCL = (CXCL - 1.5) 0.01$$

$$VBX = 0.45, \quad DXBT = (VB - 0.65) A_{10}$$

If VB is less than the minimum

$$VBX = 0.0, \quad DXBT = 0.0$$

$$\begin{aligned} C_X = & a_1 + a_2 (VNX - 2.5) + a_3 (VNX - 2.5)^2 \\ & + a_4 (VNX - 2.5)^3 + a_5 (CXCLL) + a_6 (CXCLL)^2 \\ & + a_7 (VBX) + a_8 (CRAT) + a_9 (CRAT)^2 \\ & + a_{11} (CBD) + a_{12} (CDM) - (BOOM/1.36)^2 0.01 \\ & - DXBT - DXN + DXCL \end{aligned}$$

The "IF" statements are required to circumvent the need for higher order polynomials in the equations. In this manner only linear extrapolation and interpolations are allowed on the fringes of the program capabilities. This should prevent completely erroneous estimates.

Normal Force Coefficient Derivative, Pitching Moment Coefficient Derivative and Normal Force Center of Pressure

if $0 < V_N < 3.0$ set $V_{NX} = V_N$, $D_{NX} = 0.0$

if $0 < V_B < 1.0$ set $V_{BNP} = V_B^A$, $V_{BMP} = V_B^B$, $V_{BX} = V_B$

where: Subsonic $A = 1.0$, $B = 0.8$

Supersonic $A = 1.5$, $B = 1.0$

if V_N or V_B are greater than the maximum

set $V_{NX} = 3.0$, $D_{NX} = V_N - 3.0$

$V_{BX} = 1.0$, $V_{BNP} = V_B^{0.5}$, $V_{BMP} = V_B^{0.5}$

Now set

$CV_{NN} = V_{NX} - 2.47$

$CX_{LL} = V_L - V_N - V_B - 2.15$

$CD_{MM} = D_M - 0.17$

$CB_{BD} = B_D - 1.04$

$CC_{RT} = V_N^2 / OR - 0.48$

$VB_{TI} = CV_L / 4.7$

$CN_{AB} = B_1 + B_2 (CV_{NN}) + B_3 (CX_{LL}) + B_4 (CC_{RT}) + B_5 (CV_{NN})^2 + B_6 (CX_{LL})^2$

$CN_{BT} = B_7 (V_{BNP}) + B_8 (V_{BX} \cdot CV_{NN}) + B_9 (V_{BX} \cdot CX_{LL})$

$CN_{AT} = CN_{AB} + CN_{BT}$

$$\begin{aligned}
AMOMSQ = & CNAB [C_1 + C_2 (CVNN) + C_3 (CVNN)^2 \\
& + C_4 (CVNN)^3 + C_5 (CXLL) + C_6 (CXLL)^2 \\
& + C_7 (CXLL)^3 + C_8 (CCRT) + C_9 (CCRT)^2 \\
& + C_{10} (CDMM) + C_{11} (CCRT \cdot CVNN) + C_{17} (DNX)]
\end{aligned}$$

$$\begin{aligned}
AMOMBT = & VBTT [C_{12} (VBMP) + C_{13} (VBX \cdot CVNN) \\
& + C_{14} (VBX \cdot CXLL) + C_{15} (VBX \cdot CCRT) \\
& + C_{16} (VBX \cdot CCRT \cdot CVNN)]
\end{aligned}$$

$$CPN = (AMOMSQ + AMOMBT)/CNAT$$

$$C_{N_\alpha} = CNAT$$

$$C_{M_\alpha} = (VCG - CPN) C_{N_\alpha}$$

Yaw Axial Force Coefficient

$$CXCL = VL - VN - VB - 1.5$$

$$CRAT = VN^2/OR - 0.40$$

$$CVB = VB$$

$$C_{X_2} = D_1 + D_2 (CXCL) + D_3 (CRAT) + D_4 (CVB) - C_{N_\alpha}$$

The Yaw Drag coefficient may be computed by adding C_{X_2} and C_{N_α} .

Magnus Force Coefficient Derivative, Magnus Moment Coefficient Derivative,
Magnus Force Center of Pressure

$$CVL = VL$$

$$CVB = VB$$

$$CXCL = VL - VN - VB - 1.5$$

$$CVN = VN - 2.5$$

$$CYPA = E_1 (CVL) - 0.1 (CVB)$$

at $\bar{\alpha} = 1.0^\circ$

$$CNPAN = -E_1 (CVL) [E_2 + 0.55 (CXCL) + 0.80 (CVN)] \\ + CVB (CVL/4.7)$$

$$CPF_{(1)} = -CNPAN/CYPA$$

$$C_{Yp\alpha} = CYPA$$

$$C_{n_{p\alpha(1)}} = (VCG - CPF_{(1)}) C_{Yp\alpha}$$

at $\bar{\alpha} = 2.0^\circ$

$$CNPAN = -E_1 (CVL) [E_3 + 0.55 (CXCL) + 0.80 (CVN)] \\ + CVB (CVL/4.7)$$

$$CPF_{(2)} = -CNPAN/CYPA$$

$$C_{Yp\alpha} = CYPA$$

$$C_{n_{p\alpha(2)}} = (VCG - CPF_{(2)}) C_{Yp\alpha}$$

at $\bar{\alpha} = 5.0^\circ$

$$CNPAN = -E_1 (CVL) [E_4 + 0.55 (CXCL) + 0.80 (CVN) + CVB (CVL/4.7)]$$

$$CPF_{(5)} = -CNPAN/CYPA$$

$$C_{Yp\alpha} = C_{YPA}$$

$$C_{n_{p\alpha}(5)} = (VCG - C_{PF(5)}) C_{Yp\alpha}$$

Damping Moment Coefficient

$$CLL = VL - 5.0$$

$$CCG = VCG - 3.0$$

$$CVB = VB$$

$$\begin{aligned} C_{m_q} = & -5.093 [F_1 + F_2 (CLL) + F_3 (CLL^2) + F_4 (CCG) \\ & + F_5 (CCG) (CLL) + F_6 (CCG) (CLL^2) + F_7 (CCG) (CVB) \\ & + F_8 (CVB)] \end{aligned}$$

Spin Deceleration Coefficient

$$C_{l_p} = G1 (VL/5.51)$$

Stability Analysis

The methods used for stability computations were extracted from references 44 and 45. They are identical to those contained in the original SPINNER.

Gyroscopic Stability Factor, s_g

$$s_g = 2I_x^2 p^2 / \pi I_{yp} C_{m_\alpha} d^3 v^2$$

Dynamic Stability Factor, s_d

$$s_d = \frac{2(C_{N_\alpha} - C_X + (k_1^{-2}/2) C_{n_{p\alpha}})}{(C_{N_\alpha} - C_X - (k_2^{-2}/2) C_{m_q} + (k_1^{-2}/2) C_{l_p}}$$

Nutation, Precession Frequencies $\omega_{1,2}$

$$\omega_{1,2} = \frac{pI_x}{2I_y} (1 \pm \sigma)$$

Nutation, Precession Yaw Damping Rates, $\lambda_{1,2}$

$$\lambda_{1,2} = \frac{\rho A}{4m} \left[-C_{N_\alpha} \left(1 \pm \frac{1}{\sigma} \right) + (k_2^{-2}/2) \left(1 \pm \frac{1}{\sigma} \right) C_{m_q} \pm (k_1^{-2}/\sigma) C_{n_{p\alpha}} \right]$$

where

$$k_1^{-2} = md^2/I_x$$

$$k_2^{-2} = md^2/I_y$$

$$\sigma = \sqrt{1 - 1/s_g}$$

The dispersion (DISP) is the radius in mils of a circle which a projectile will impact in a vertical plane when disturbed to a first maximum yaw angle of 5 degrees or less. The basis for this calculation is derived in Reference 71.

The time step (DELT) shown will provide 20 integrations per nutation cycle. This is entirely adequate for a 4th Order Range Kutta integrator.

RESULTS AND DISCUSSIONS

The results of several test cases are presented in Figures 2 thru 15. Plotted are experimental points, SPIN-69 and SPIN-73 results. Tabulated outputs of SPIN-73 are shown as tables 2 thru 15.

The following ranges of parameters are demonstrated by the test cases.

Total length	3.8 thru 10.0 calibers
Nose length	1.6 thru 5.5 calibers
Boattail length	0.0 thru 1.0 calibers
Ogive radius	tangent thru conical
Meplat diameter	0.0 thru 0.26 calibers
Band diameter	1.00 thru 1.05 calibers

In general the correlations between SPIN-73 and the experimental data is very good with noticeable improvements over SPIN-69. Most of the effort during this current study has been directed at the Axial Force and Pitching Moment correlations as these two coefficients are by far the most accurately determined during the experimental process. Much work still remains to be done on these coefficients in terms of defining a more adequate empirical model.

The most poorly determined coefficients remain the Magnus and damping. It is this author's opinion that the SPIN-73 improvement in these the calculations is negligible. While some new data has been published since 1968, in general data was previously available on similar shapes. For example the projectiles referred to as the XM380 and XM549 were experimentally

investigated long ago as the T388 and T387. This data was available in 1967 and had been included in the original (SPIN-69) program.

The bulk of the data published by AEDC through calendar year 1972 is suspect as far as the Magnus and damping coefficient are concerned because the effect on linear theory reductions of a slowly varying $pd/2V$ was not taken into account.

This author also found in several instances as did Sears that the geometric description of the projectiles under test were not available either in the data reports or the data files.

The probable errors to the experimental data of the SPIN-73 empirical equations are shown in Table 1. The number of data points used to compute the probable error is shown in parenthesis.

CONCLUSIONS AND RECOMMENDATIONS

The SPIN-73 program has been shown through test cases to be more accurate than the SPIN-69 program.

The updating of SPIN-73 should be continued as new data is accumulated.

Records should be kept of shortcomings and extremely poor predictions.

Data should be more carefully reported with respect to actual configuration tested.

REFERENCES

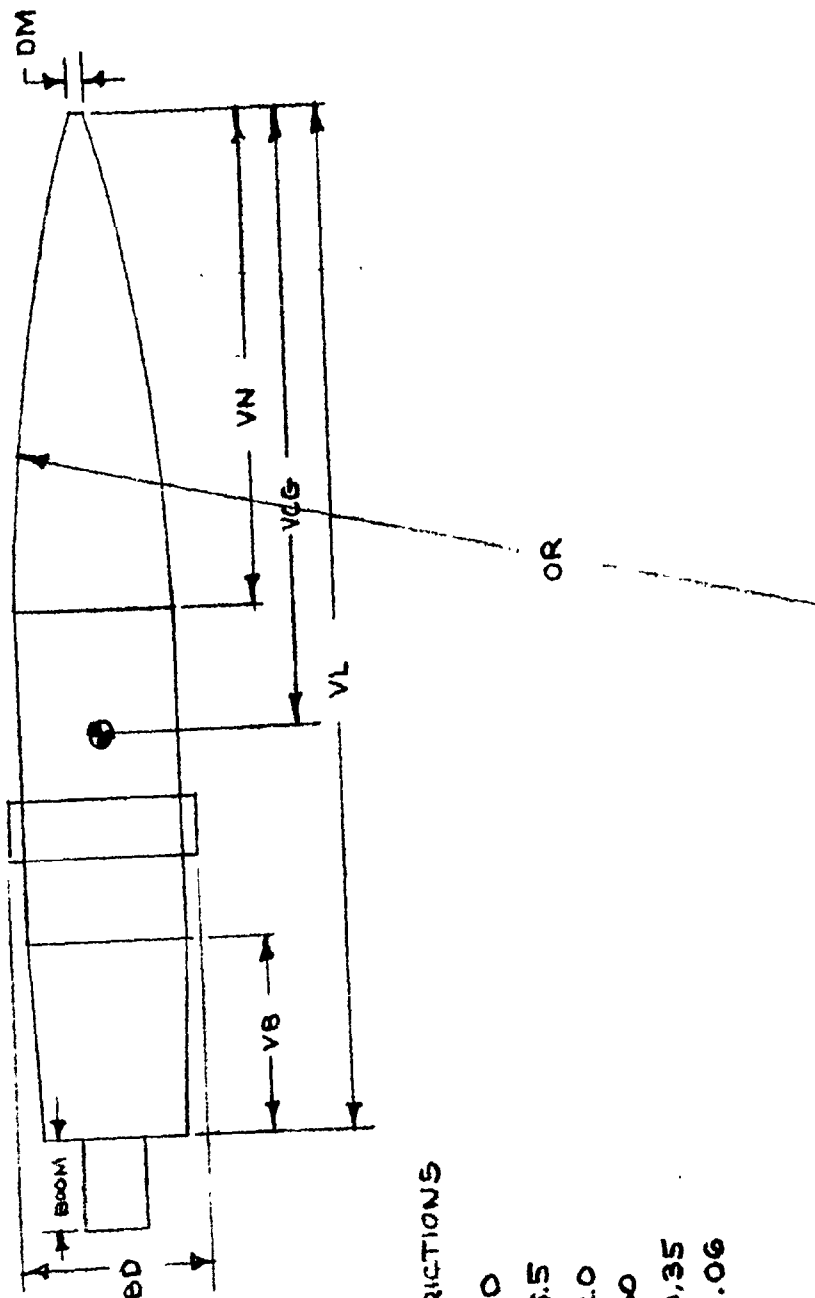
1. Ballistics Research Laboratories, Free Flight Aerodynamics Branch Firing Records (Unpublished).
2. Boyer, E. Aerodynamics Characteristics for Small Yaws of 20mm Shell HEI, T282E1 with Fuze M505 for Mach No. .36 to 2.78. BRL Memo Report 916, August 1955. AD077515.
3. Boyer, E. Comparison of the Aerodynamic Characteristics of the 20mm HEI, T282E1 Shell with Fuze M505 and Fuze T821. BRL Technical Note 1055, December 1955. AD084726.
4. Boyer, E. Aerodynamic Characteristics of 20mm Shell. HEIT282E1. BRL Memo Report 813, July 1954. AD044114.
5. Boyer, E. Some Aerodynamic Properties of Three 105mm Shells, M1, T377 and T107. BRL Memo Report 1144. April 1958, AD162924.
6. Boyer, E. Aerodynamic Properties of a 105mm Model of the 8 Inch T347E1. BRL Memo Report 1212, June 1959. AD220559.
7. Boyer, E. Free Flight Range Test of a 10-Caliber Cone Cylinder. BRL Memo Report 1258, April 1960. AD2373579.
8. Boyer, E. Comparison of Aerodynamic Characteristics of Live and Inert 70mm T231 Gun-Boosted Rockets. BRL Memo Report 1086, July 1957. AD144336.
9. Boyer, E. Aerodynamic Properties of the 90mm M-71 Shell. BRL Memo Report 1475, April 1963. AD411804.
10. Boyer, E. A Limited Aerodynamic Test of a 175mm Extended Range Subcaliber Projectile. BRL Memo Report 2160, March 1972.
11. Boyer, E. Comparison of Aerodynamic Characteristics of 20mm HEI Shell M97 with Fuze M75 and 20mm Shell T226E1. BRL Memo Report 865, April 1955. AD069009.
12. Brandon, F.J. Aerodynamic Properties of the 152mm XM617 Projectile. BRL Memo Report 1998, July 1969. AD857512.
13. Brandon, F.J. Aerodynamic Characteristics of the 152mm Ammunition XM409E5, XM411E3, XM657E2 at Small Yaw. BRL Memo Report 2024, February 1970. AD866668.
14. Braun, W.F. Aerodynamic Data for Small Arms Projectiles. BRL Report No. 1630, January 1973.
15. Buford, W.E. Aerodynamics Characteristics of 20mm Shell T282E1. BRL Memo Report 834, October 1954. AD064653.

16. Buford, W.E. Aerodynamic Characteristics of the 30mm Shell T306E10. BRL Technical Note 1019, July 1955. AD077533.
17. Carman, J.B. Wind Tunnel and Free Flight Range Tests of 3 and 5 Caliber AN Spinner Projectile with Rotation Bands. AEDC-TR-71-119, June 1971.
18. Deitrick, R.E. Effect of a Hemispherical Base on the Aerodynamic Characteristics of Shell. BRL Memo Report 947, November 1955. AD095782.
19. Dickinson, E.R. The Zero-Yaw Drag Coefficient for Projectile 8-Inch, HE, M106. BRL Memo Report 1681, September 1965. AD473562.
20. Dickinson, E.R. Some Aerodynamic Coefficients for Projectile 4.2 Inch: HE, M329A1. BRL Memo Report 1900, February 1968. AD8227762.
21. Dickinson, E.R. Stability Determination of the 152mm Heat/mp Shell XM409E4. BRL Technical Note 1404, May 1961. AD374985.
22. Dickinson, E.R. Stability Determination of the 152mm Heat-mp-T Shell XM409F5 Mod 2A. BRL Memo Report 1391, February 1962. AD329235.
23. Dickinson, E.R. Zero-Yaw Drag Coefficient for Projectile 175mm HE M437. BRL Memo Report 1568, March 1964. AD443811.
24. Dickinson, E.R. Some Aerodynamic Effect of Varying the Body Length and Head Length of a Spinning Projectile. BRL Report 1664, July 1965. AD469897.
25. Dickinson, E.R. The Effect of Boattailing on the Drag Coefficient of Cone-Cylinder Projectile at Supersonic Velocity. BRL Memo Report 842, October 1954. AD057769.
26. Dickinson, E.R. Some Aerodynamic Effects of Head Shape Variation at Mach 2.44. BRL Memo Report 838, October 1954. AD057748.
27. Dickinson, E.R. Some Aerodynamic Effects of Blunting a Projectile Nose. BRL Memo Report 1596, September 1964. AD451977.
28. Dickinson, E.R. The Zero Yaw Drag Coefficient for Projectile 155mm; Atomic XM454. BRL Memo Report 1757, June 1966. AD488057.
29. Donovan, W.F. Analysis of Free Flight Test of 107mm Mortar Projectile XM571 RAP. BRL Memo Report 2013, October 1969. AD862137.
30. Donovan, W.F. Transonic Range Tests of 5 Inch/38 Rocket Assisted Projectile (Inert). BRL Memo Report 2071, November 1970. AD878280.
31. Donovan, W.F. Transonic Range Tests of 5 Inch/54 Rocket Assisted Projectile (Inert). BRL Memo Report 2107, July 1971. AD730661.

32. General Electric Company, Advance Munitions Development Burlington, Vermont, Aerodynamic Data Files (Unpublished).
33. Haseltine, W.R. Yawing Motion of 5"0 MK41 Projectile Studies By Means of Yaw Sonde. NWCTP4779, August 1969. AD862065.
34. Hitchcock, H.P. Aerodynamic Data for Spinning Projectiles. BRL Report 620, January 1952. AD800469.
35. Karpov, B.G. The Aerodynamic Properties of the 155mm Shell M101 from Free Flight Range Tests of Full Scale and 1/12 Scale Model. BRL Memo Report 1582, June 1964. AD454925.
36. Karpov, B.G. Aerodynamic Characteristic of the 110mm HE, T194 Shell and its Modifications with Fuze M51A5. BRL Memo Report 1057, February 1957. AD127627.
37. Karpov, B.G. The Effect of Various Boattail Shapes on Base Pressure and Other Aerodynamic Characteristics of a 7-Caliber Long Body of Revolution at M=1.70. BRL Memo Report 1295, August 1965. AD474352.
38. Karpov, B.G. Aerodynamic Characteristic of the 175mm T203 Shell and the 175mm Square Base Shell with Fuze M51A5. BRL Memo Report 956, December 1955. AD086528.
39. Krial, K.S. Aerodynamic Properties of a Family of Shells of Similar Shape; 105mm XM380E5, XM380E6, T388 and 155mm T387. BRL Memo Report 2023, February 1970. AD866610.
40. MacAllister, L.C. A Compendium of Ballistic Properties of Projectiles of Possible Interest in Small Arms, BRL Report 1532, February 1971.
41. MacAllister, L.C. Aerodynamic Properties of the 2.75 Inch Rocket T131. BRL Memo Report 948, November 1955. AD085539.
42. MacAllister, L.C. The Aerodynamic Properties and Related Dispersion Characteristics of a Hemispherical Base Shell, 90mm, HE, T191 with and Without Tracer Element. BRL Memo Report, March 1956. AD094833.
43. Murphy, C.H. The Effect of Length on the Aerodynamic Characteristics of Bodies of Revolution in Supersonic Flight. BRL Report 876, August 1953. AD021307.
44. Murphy, C.H. Free Flight Motion of Symmetric Missiles. BRL Report 1216, July 1963, AD442757.
45. Nicolaides, J.D. Free Flight Dynamics, Univ. of Notre Dame 1968.
46. Odem, C.T. A Revised Drag Coefficient, KD Based on the 8 Inch Howitzer Shell, HE M106. BRL Memo Report 1065, April 1957, AD132170.

47. Odem, C.T. Drag Coefficient of HE Shell for the New Series of Field Artillery Weapons. BRL Memo Report 1013, July 1956. AD105611.
48. Picatinny Arsenal, Dover, New Jersey, Aeroballistics Branch Files.
49. Piddington, M.J. The Aerodynamic Properties of a Caliber .223 Remington Bullet Used in the M16 (AR15) Rifle. BRL Memo Report 1758, June 1966. AD489960.
50. Piddington, M.J. Comparitive Evaluation of the 20mm Developmental Ammunition - Exterior Ballistics. BRL Memo Report 2193, May 1972.
51. Piddington, M.H. Deformation Characteristic of One Lot (LC SP412) of 5.56mm M-193 Ammunition. BRL Memo Report 2016, October 1969. AD862966.
52. Piddington, M.H. Some Aerodynamic Properties of a Low Velocity Projectile with a Hemispherical Nose and L/D of 4.3. BRL Memo Report 1639, April 1965. AD472371.
53. Piddington, M.H. Aerodynamic Properties of a 20mm HE-T Projectile for VRFWS. BRL Memo Report 2000, July 1969. AD859054.
54. Piddington, M.H. Aerodynamic Characteristic of the 7.62mm NATO Ammunition M-59, M-80, M-61, M-62. BRL Memo Report 1833. March 1967. AD815788.
55. Roecker, E. Large Yaw Firings of the 20mm HEI, T282E1 Shell with Fuze T196 at Mach Number 2.3. BRL Memo Report 888, April 1955. AD068718.
56. Roecker, E. Aerodynamic Characteristics of 30mm HEI Shell T306 E10. BRL Memo Report 1098, August 1957. AD152952.
57. Roecker, E. The Aerodynamic Properties of the 105mm HE Shell, M1 in Subsonic and Transonic Flight. BRL Memo Report 929, September 1955. AD078604.
58. Roschke, E.J. The Effect Nose Truncation on the Aerodynamic Properties of the 9 Caliber AN Spinner Rocket Near Sonic Velocity. BRL Technical Note 902, May 1954. AD061551.
59. Roschke, E.J. The Drag and Stability Properties of the Hemispherical Base Shell, 75mm, T50E2. BRL Memo Report 927, September 1955. AD079488.
60. Sears, E.S. An Empirical Method for Predicting Aerodynamic Coefficients for Projectiles - Drag Coefficient, AFATL-TR-72-173, August 1972.
61. Schmidt, L.E. The Dynamic Properties of Pure Cone and Cone Cylinders. BRL Memo Report 759, January 1954. AD030249.
62. Schmidt, L.E. The Aerodynamic Properties of the 7-Caliber Army-Navy Spinner Rocket in Transonic Flight. BRL Memo Report 775, March 1954. AD035840.
63. Schmidt, L.E. Aerodynamic Properties of 4.9 Calibers Long, Square Based Shell at Transonic Speeds. BRL Memo Report 824, August 1954. AD047993.

64. Scott, W.E. The Effect of a Rotating Band upon Some Aerodynamic Coefficient of the Seven Caliber AN Spinner Rocket at M=1.8. BRL Memo Report 1302, September 1960. AD246223.
65. Scott, W.E. Some Aerodynamic Properties of a 105mm Model of the 155mm T-358 Shell. BRL Memo Report 1369, September 1961. AD267268.
66. Watt, R.M. Free Flight Range Tests of Blunted 4, 4.5, and 5 Caliber Bodies of Revolution with Secant-Ogive, Tangent-Ogive, and Conical Nose Shapes. AEDC-TR-71-166, December 1971.
67. Watt, R.M. Free Flight Range Tests of an Improved 20mm Shell. AEDC-TR-70-289, January 1971.
68. Whyte, R.H. Spinner - A Computer Program for Predicting the Aerodynamic Coefficient for Spin Stabilized Projectiles. General Electric TIS 69 APB3, August 1969.
69. Whyte, R.H. Effects of Boattail Angle of Aerodynamic Characteristics of 175mm M437 Projectile at Supersonic Mach Numbers. PATM 1646, September 1965.
70. Whyte, R.H. Spinner - A Computer Program for Emperically Predicting the Aerodynamic Coefficients of Spin Stabilized Projectiles, Picatinny Arsenal ESL IR 319, February 1967.
71. Whyte, R.H. Dispersion of Projectiles as a Function of Physical and Aerodynamic Properties. General Electric, Burlington, Vermont, Advance Munition Report, January 1970.
72. Winchenbach, G.L. Free Flight Range Tests of Basic and Boattail Configurations of 3 and 5 Caliber and Spinner Projectiles. AEDC-TR-70-12. March 1970.
73. Winchenbach, G.L. Free Flight Range Test of the 20mm M56A2 Shell with a Modified M505E3 Fuze. AEDC-TR-67-108, June 1967.
74. Winchenbach, G.L. Free Flight Range Tests of the 20mm M56A2 Shell with the M505E3 Fuze. AEDC-TR-65-258, January 1966.
75. Winchenbach, G.L. Free Flight Range Tests of a 25mm Shell with the M505A3 Fuze. AEDC-TR-71-62, April 1971.



DIMENSION RESTRICTIONS

$2.5 < VL < 10$
 $1.2 < VN < 5.5$
 $0.0 < VB < 2.0$
 $VN/VL < 0.9$
 $0.2 < DM < 0.35$
 $1.0 < BD < 1.06$

PROJECTILE PARAMETERS - INPUT/OUTPUT

FIGURE 1

COEFFICIENT PROBABLE ERRORS

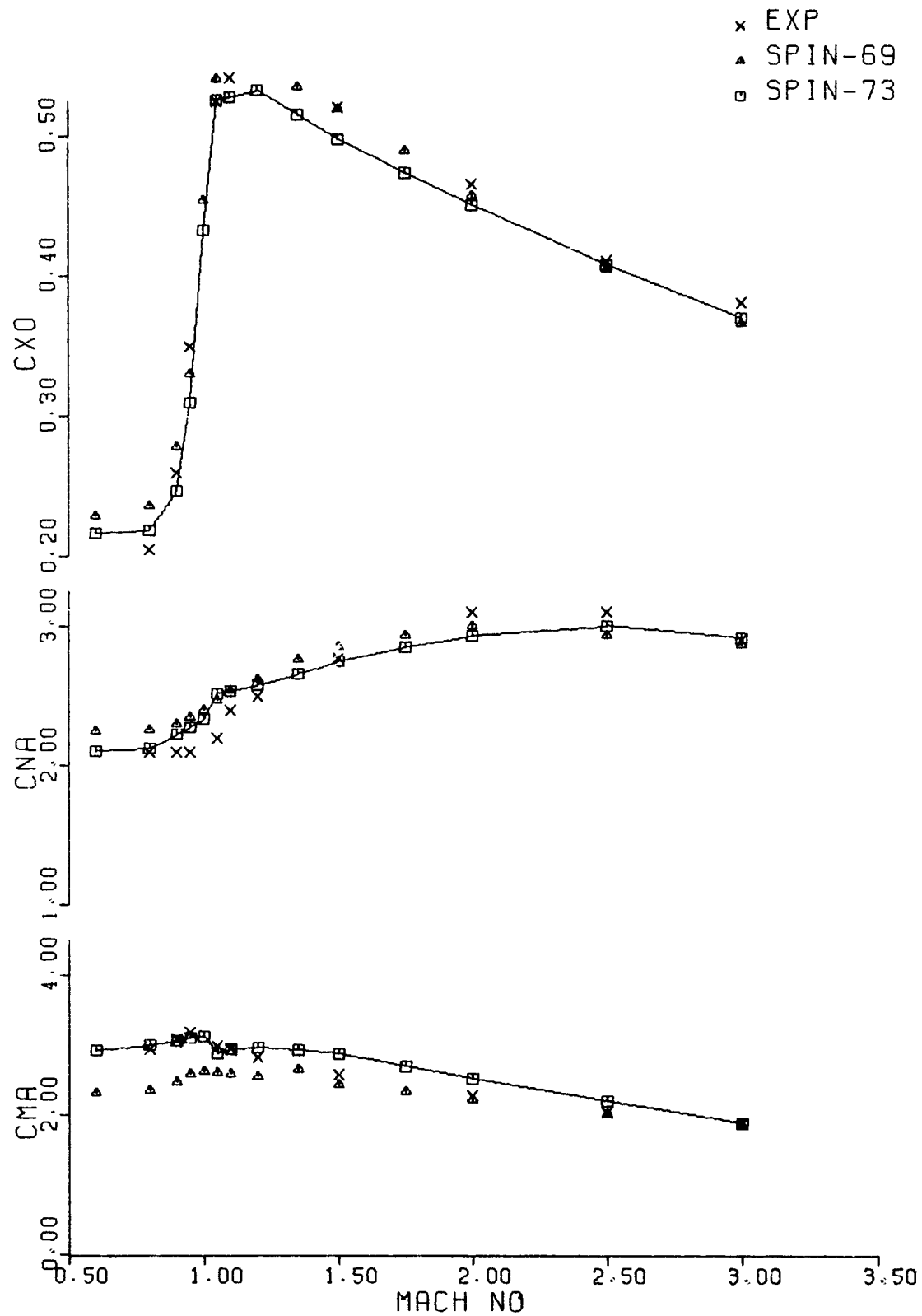
	e_{C_x}	$e_{C_{N_1}}$		$e_{C_{m_2}}$		$e_{C_{m_3}}$	$e_{C_{N_{p_2}}}$
		SQ BASE	BOATAIL	SQ BASE	BOATAIL		
0.80	0.0078 (84)*	0.06 (86)	0.10 (37)	0.15 (90)	0.11 (59)	3.0 (78)	0.18 (72)
0.90	0.0090 (62)	0.06 (86)	0.10 (37)	0.15 (90)	0.11 (39)	—	—
0.95	0.0092 (56)	0.06 (86)	0.11 (49)	0.15 (90)	0.12 (53)	—	0.16 (72)
1.05	0.0076 (111)	0.09 (129)	0.10 (49)	0.13 (138)	0.10 (54)	3.0 (78)	—
1.10	0.0076 (111)	0.09 (129)	0.10 (49)	0.13 (138)	0.10 (54)	—	0.16 (72)
1.20	0.0076 (145)	0.09 (129)	0.09 (64)	0.13 (138)	0.14 (71)	—	0.12 (59)
1.50	0.0078 (193)	0.09 (129)	0.08 (52)	0.13 (138)	0.15 (58)	3.0 (63)	0.12 (59)
2.00	0.0078 (194)	0.09 (132)	0.07 (50)	0.12 (141)	0.17 (58)	3.0 (63)	0.12 (59)
2.50	0.0072 (159)	0.09 (132)	0.06 (38)	0.12 (141)	0.17 (45)	—	0.12 (59)
3.00	0.0072 (159)	—	—	—	—	—	—

* NO. OF DATA PTS. INCLUDED IN FIT

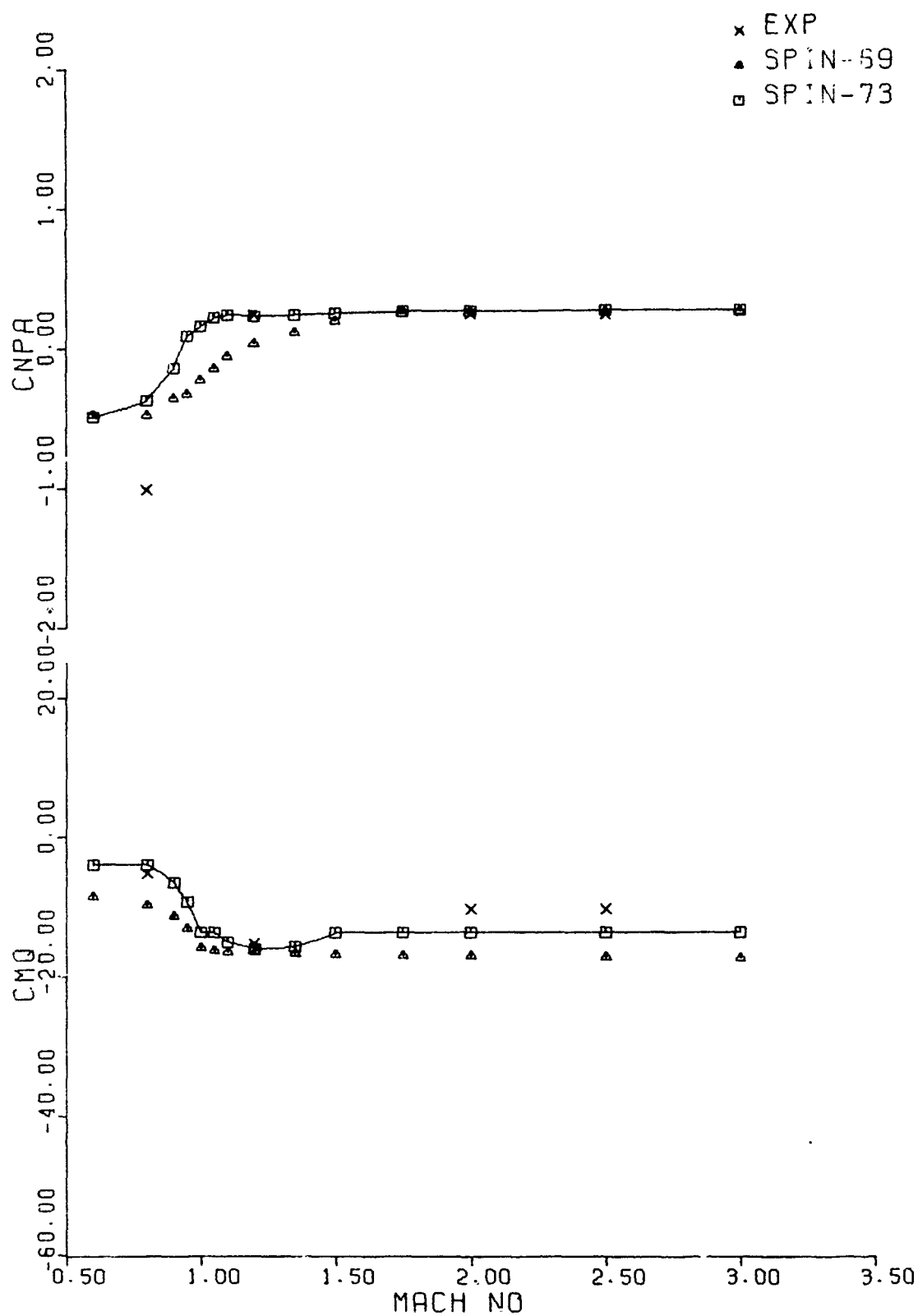
TABLE 1

[illegible]

20MM M56A3



20MM M56A3

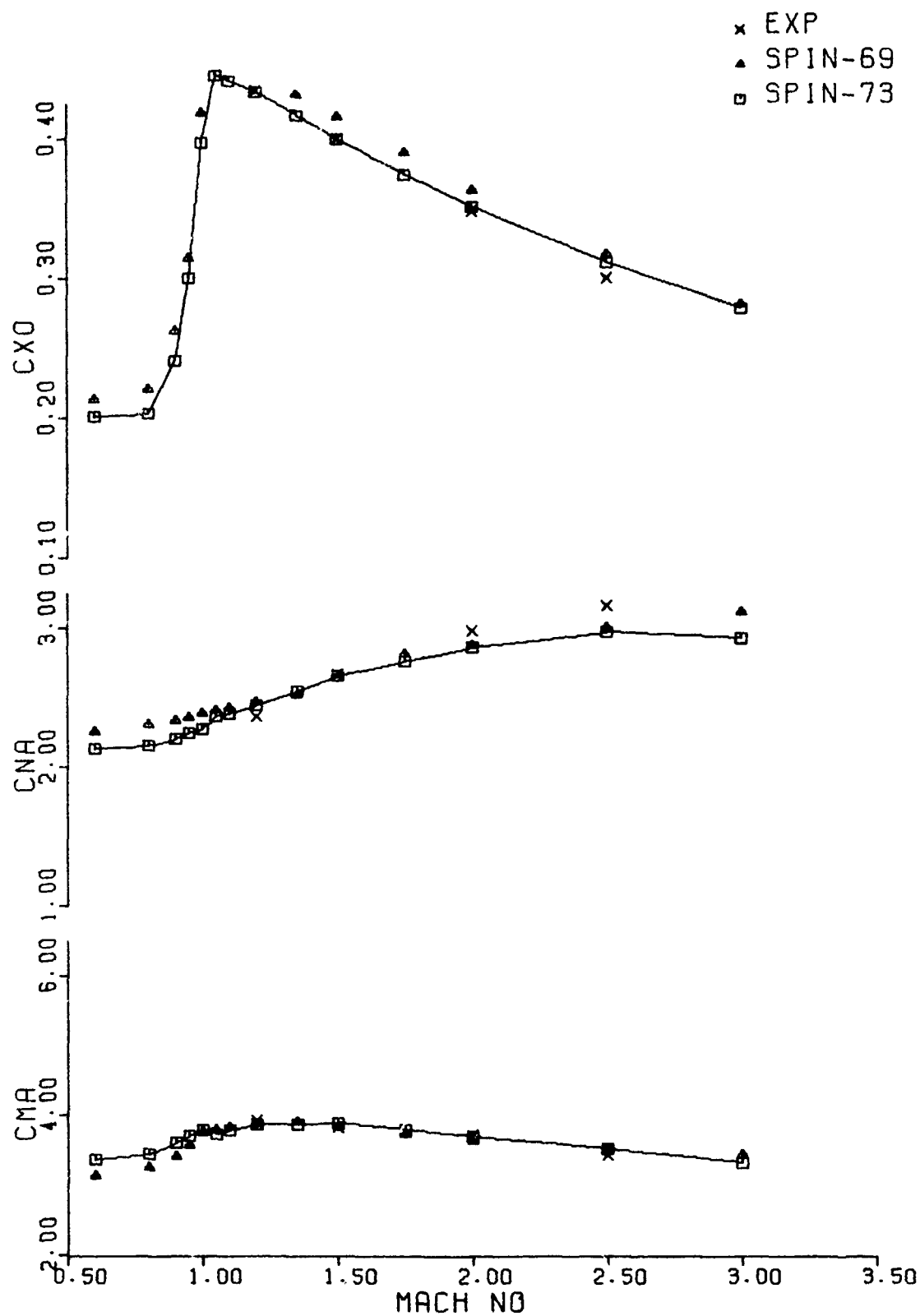


25

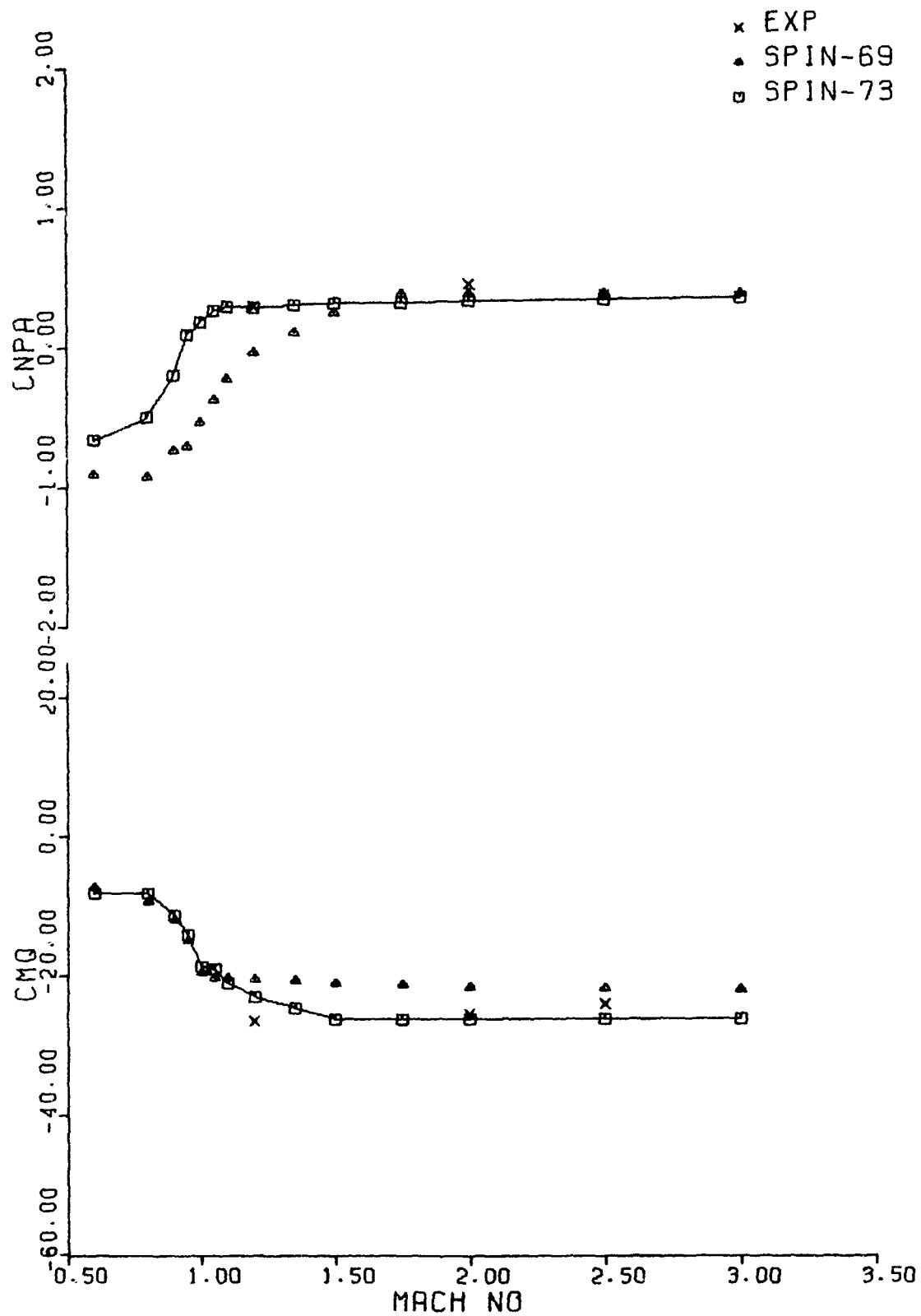
6,441318337 2140'-46" E 27

32

20MM 5 CAL ANSR



20MM 5 CAL ANSR

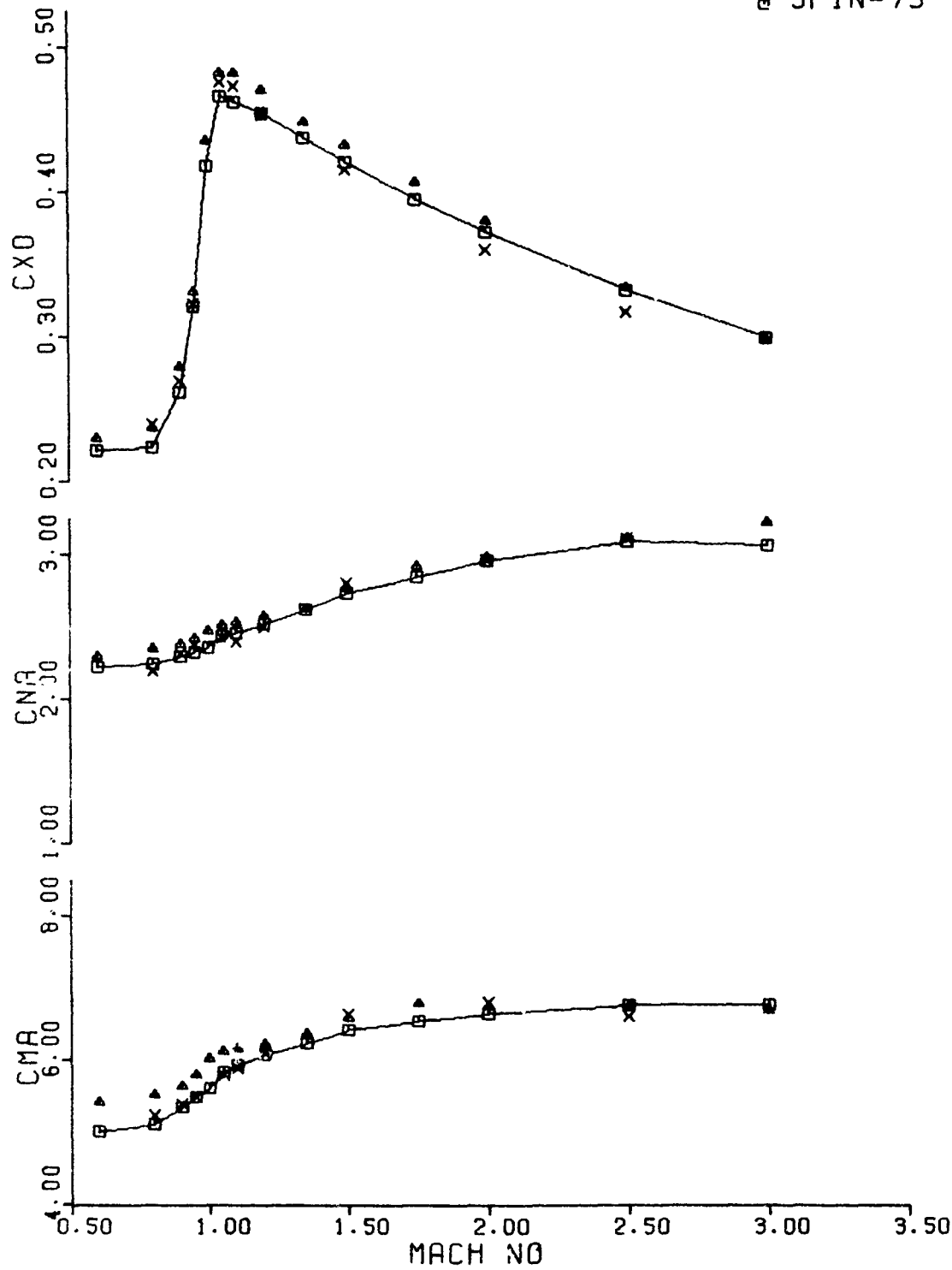


[illegible]

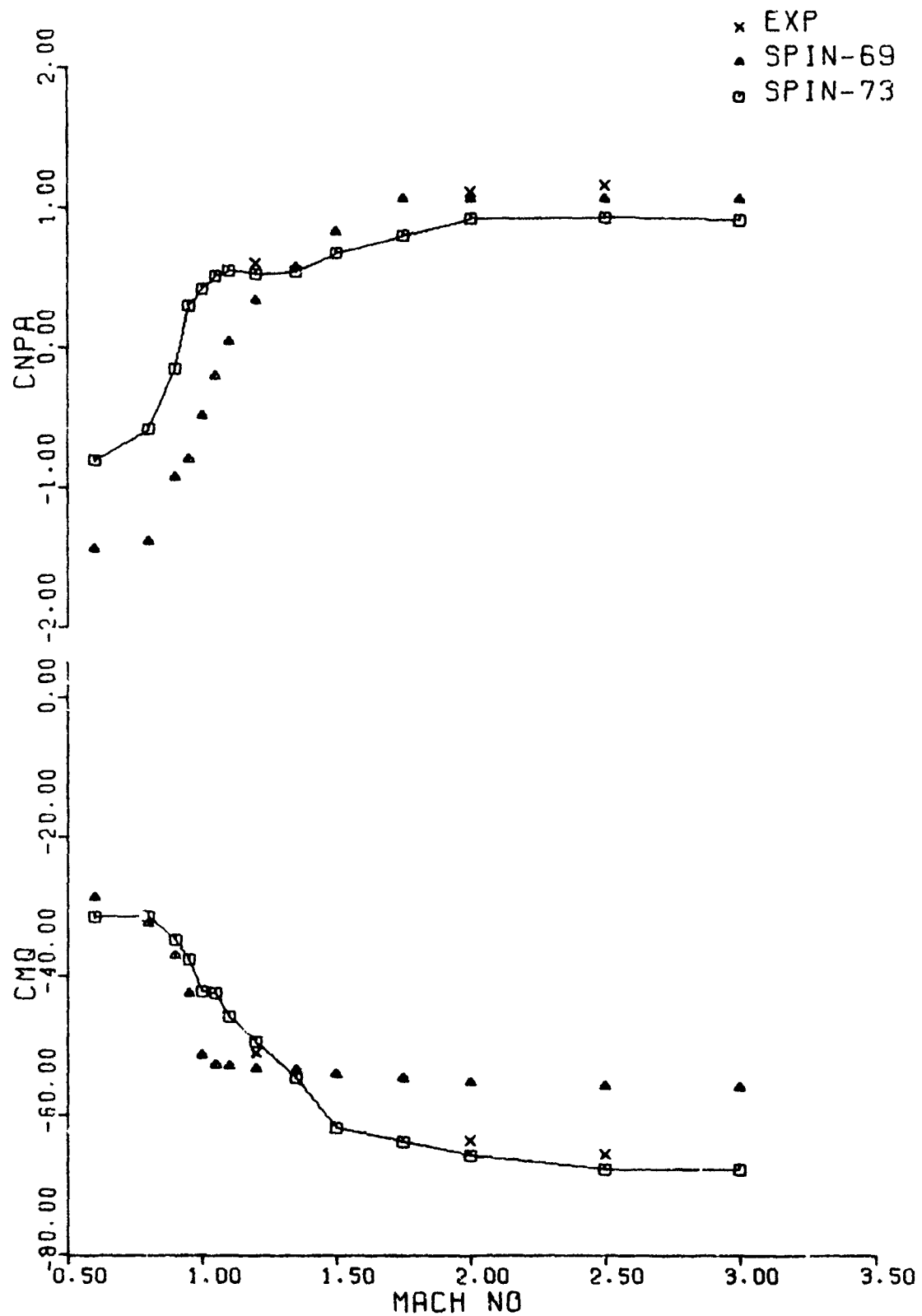
35

20MM 7 CAL ANSR

x EXP
 ▲ SPIN-69
 □ SPIN-73



20MM 7 CAL ANSR



OF BURLINGTON VERMONT
9 CAL

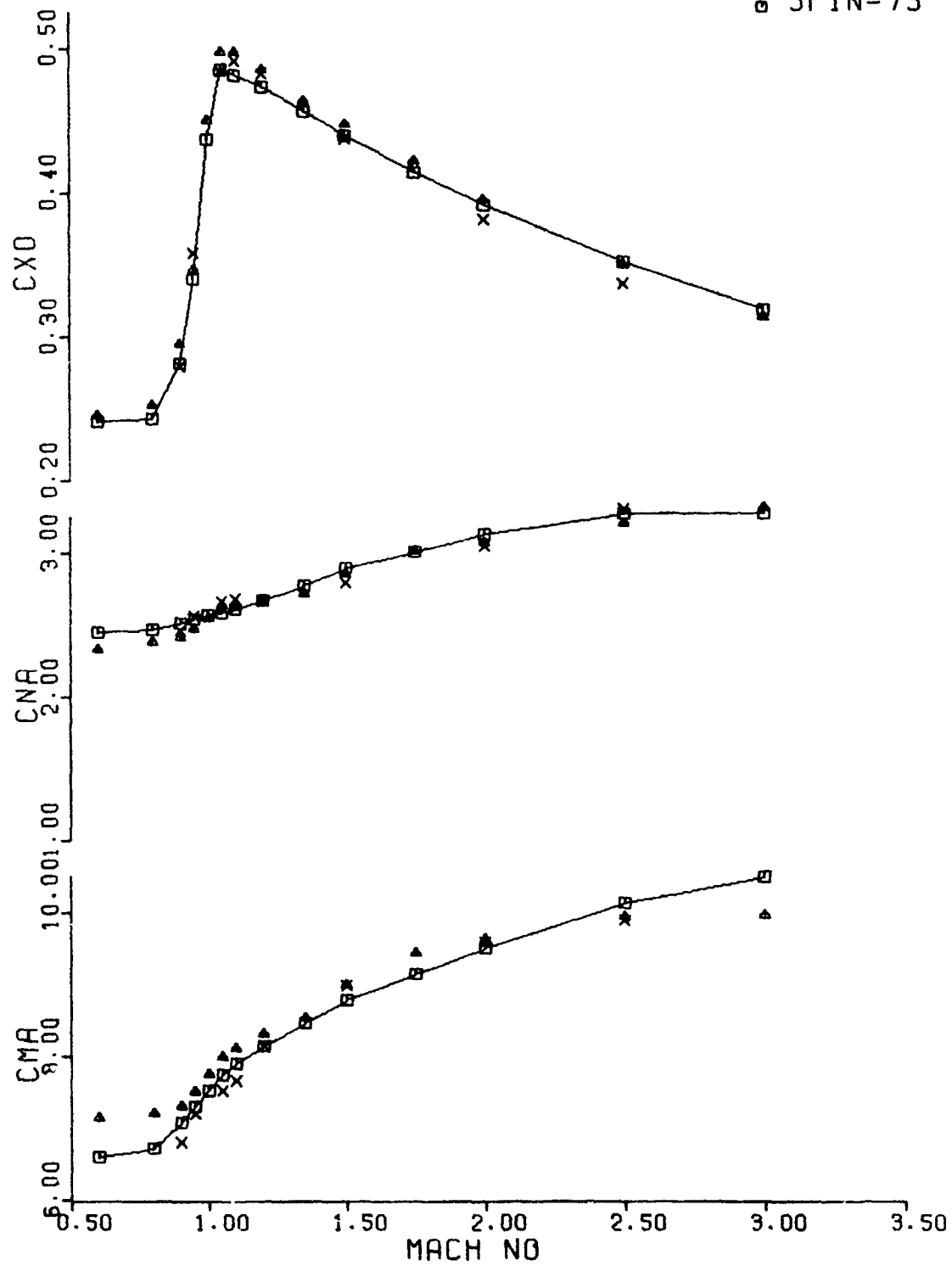
DIAMETER INCHES	IX LB-IN-SC 0.776	IX LB-IN-SC 0.000	IV LB-IN-SC 0.000	WEIGHT PS 1.000	GUN TWIST CAL/TURN 0.000	ACTUAL TWIST CAL/TURN 0.000	HAZD DIAMETER 1.000	NOSE RADIUS 8.000	TEMPERATURE DEG-F 0.000	AIR DENSITY SLUGS/FT ³ 0.00270
TOTAL LENGTH 9.000	NOSE LENGTH 2.000	HAZD LENGTH 0.000	CU (FM NOSE) 5.000	MEPLAT DIAMETER 0.000	HAZD DIAMETER 1.000	NOSE RADIUS 8.000	TEMPERATURE DEG-F 0.000	AIR DENSITY SLUGS/FT ³ 0.00270		
WACH	Gx	Gx2	CNA	CMA	CPH	CYPA	CNPA	CNPA3	CNPA5	CLP
0.010	0.242	3.445	2.460	6.503	2.765	-1.440	-0.900	175.583-1716.333	4.425	-0.59
0.600	0.242	3.445	2.460	6.628	2.764	-1.440	-0.900	175.583-1716.333	4.425	-0.59
0.800	0.244	3.935	2.480	6.772	2.736	-1.440	-0.612	150.583-1558.333	4.625	-0.57
0.900	0.282	4.400	2.525	7.110	2.234	-1.020	-0.441	116.583-1124.333	5.025	-0.48
0.950	0.341	4.882	2.555	7.330	2.179	-2.070	0.569	91.583-878.333	5.325	-0.41
1.000	0.438	5.635	2.585	7.517	2.135	-1.890	0.709	62.583-588.333	5.425	-0.39
1.050	0.486	6.411	2.594	7.746	2.056	-1.710	0.812	37.583-338.333	5.525	-0.39
1.100	0.482	7.173	2.617	7.913	2.027	-1.620	0.850	26.583-228.333	5.575	-0.39
1.200	0.474	8.166	2.684	8.140	2.010	-1.440	0.799	18.783-150.333	5.605	-0.38
1.350	0.457	7.566	2.784	8.175	2.006	-1.440	0.824	15.583-118.333	5.625	-0.38
1.500	0.440	6.946	2.904	8.801	2.020	-1.440	1.274	13.983-102.333	5.935	-0.38
1.750	0.414	6.336	3.014	9.170	2.008	-1.440	1.721	12.383-86.333	6.245	-0.37
2.000	0.391	5.715	3.135	9.522	2.012	-1.440	2.167	10.783-70.333	6.425	-0.37
2.500	0.351	5.055	3.275	10.140	1.954	-1.440	2.162	9.183-54.333	6.555	-0.36
3.000	0.318	4.279	3.266	10.508	1.833	-1.440	2.066	7.583-38.333	6.565	-0.34
4.000	0.280	3.594	3.166	10.291	1.803	-1.440	1.980	7.583-38.333	6.495	-0.33
5.000	0.258	2.909	3.066	10.048	1.773	-1.440	1.764	7.583-38.333	6.425	-0.32
									6.325	-0.33

AERODYNAMIC COEFFICIENTS

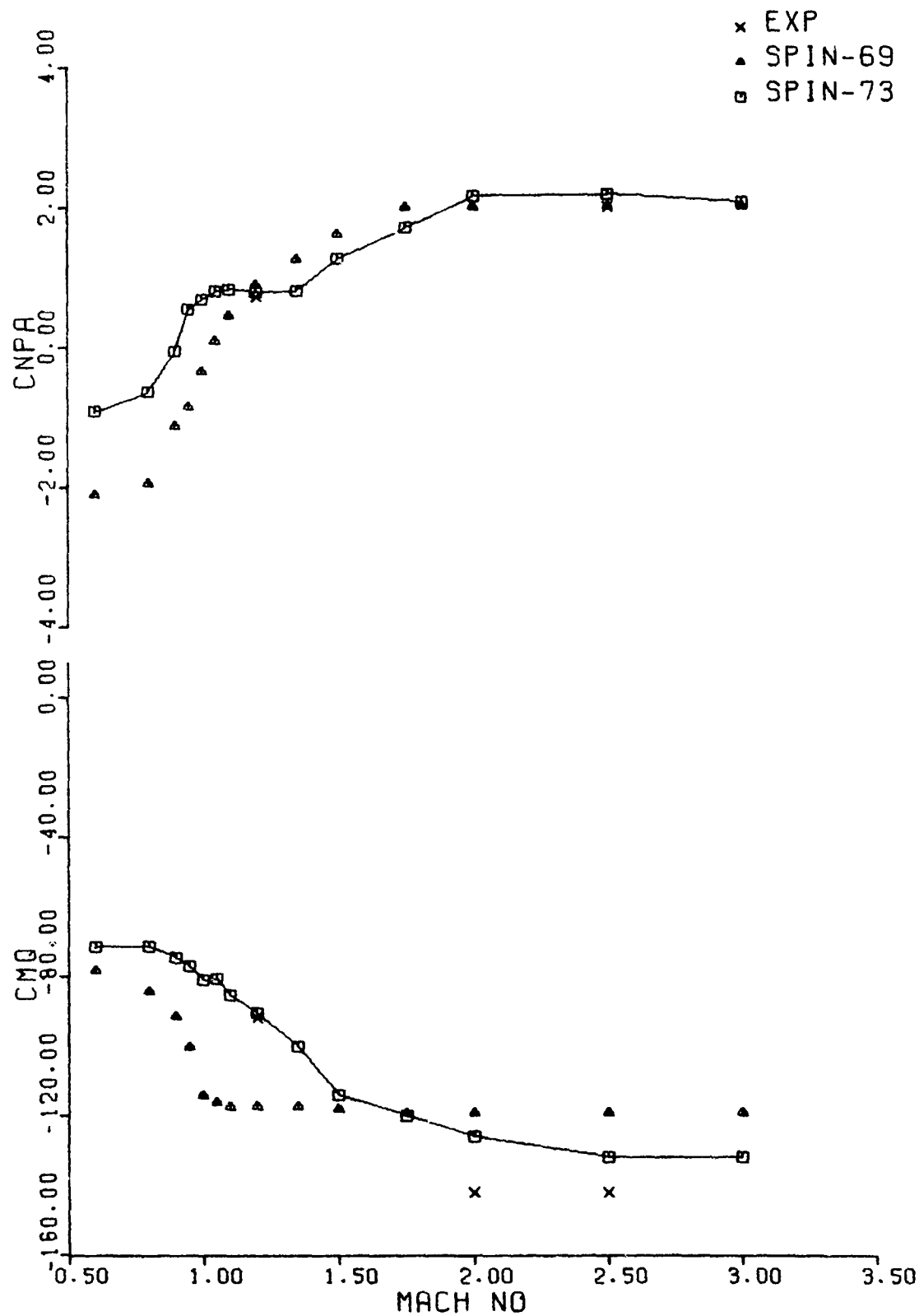
Best Available Copy

20MM 9 CAL ANSR

x EXP
 ▲ SPIN-69
 □ SPIN-73



20MM 9 CAL ANSR



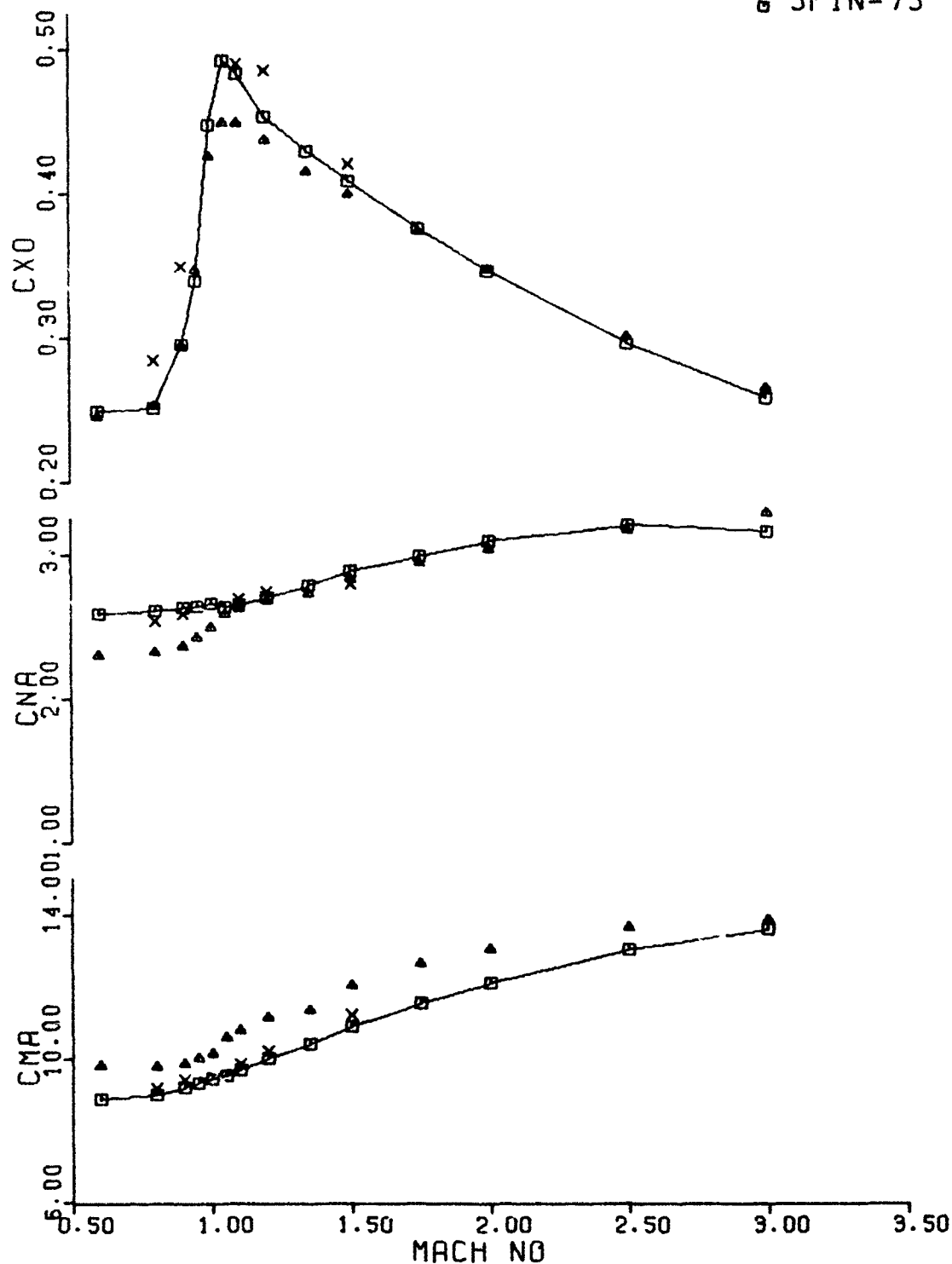
[illegible]

1. Background

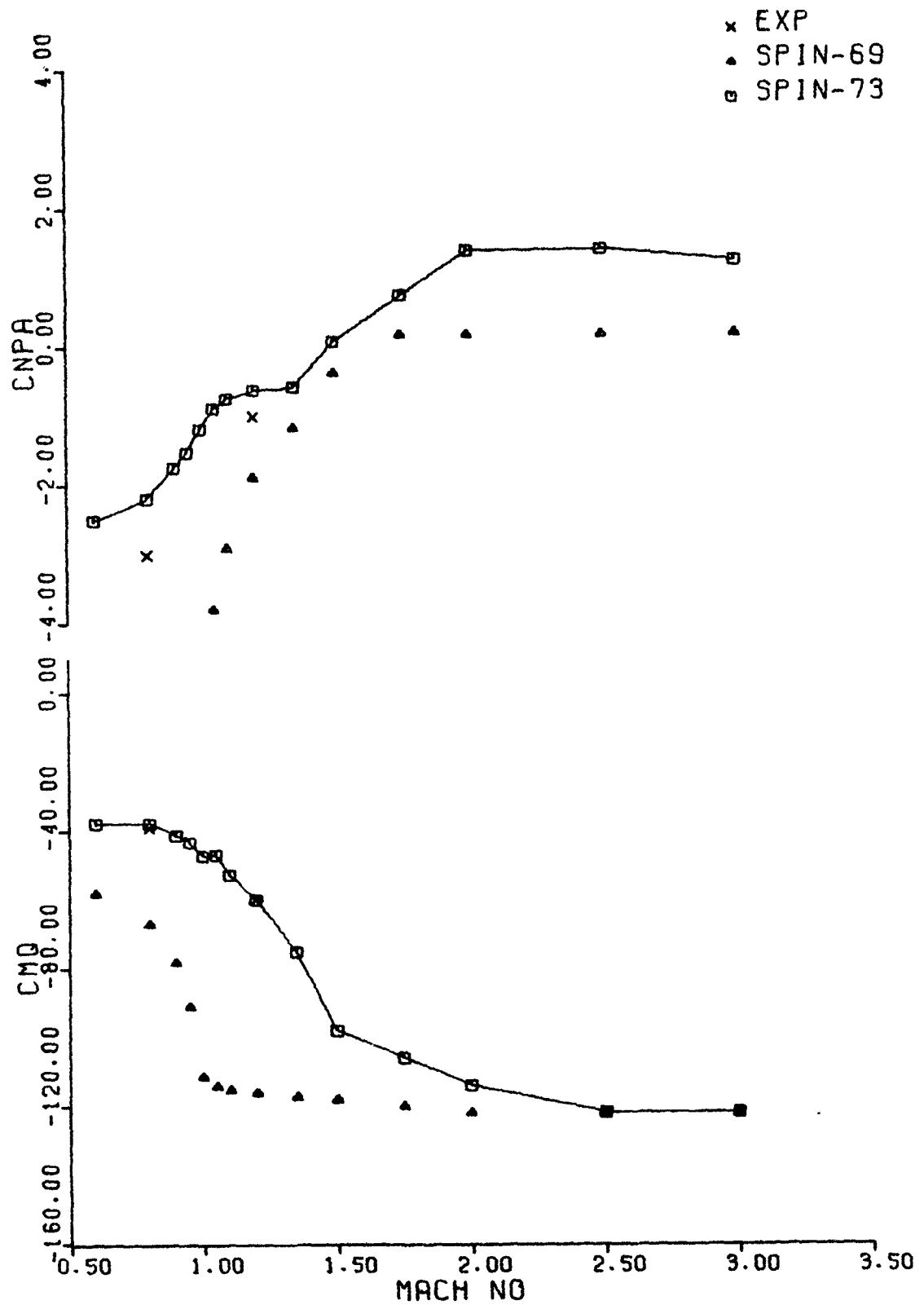
41

20MM 10 CAL CONE CYL

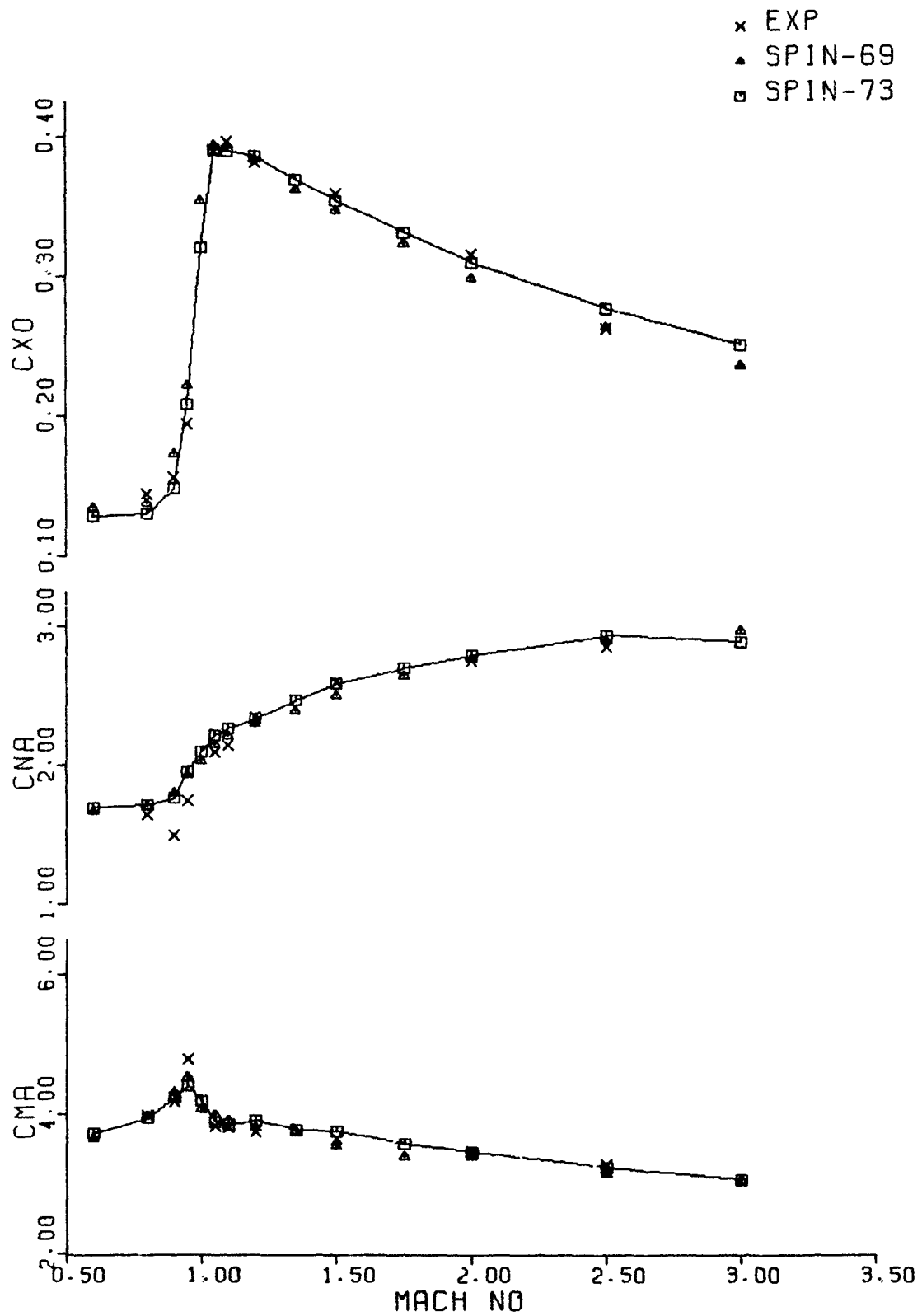
x EXP
 ▲ SPIN-69
 □ SPIN-73



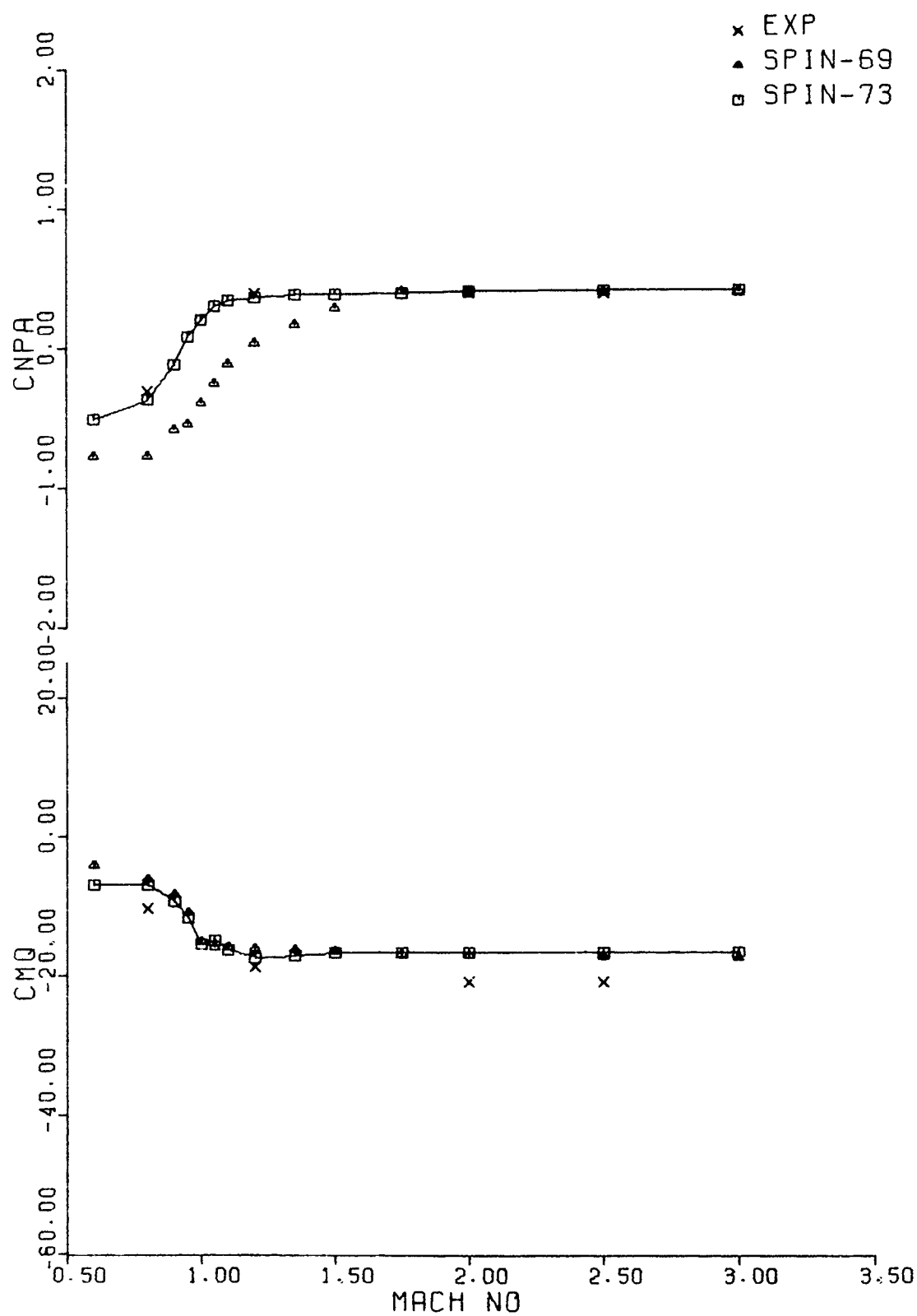
20MM 10 CAL CONE CYL



90MM M71



90MM M71

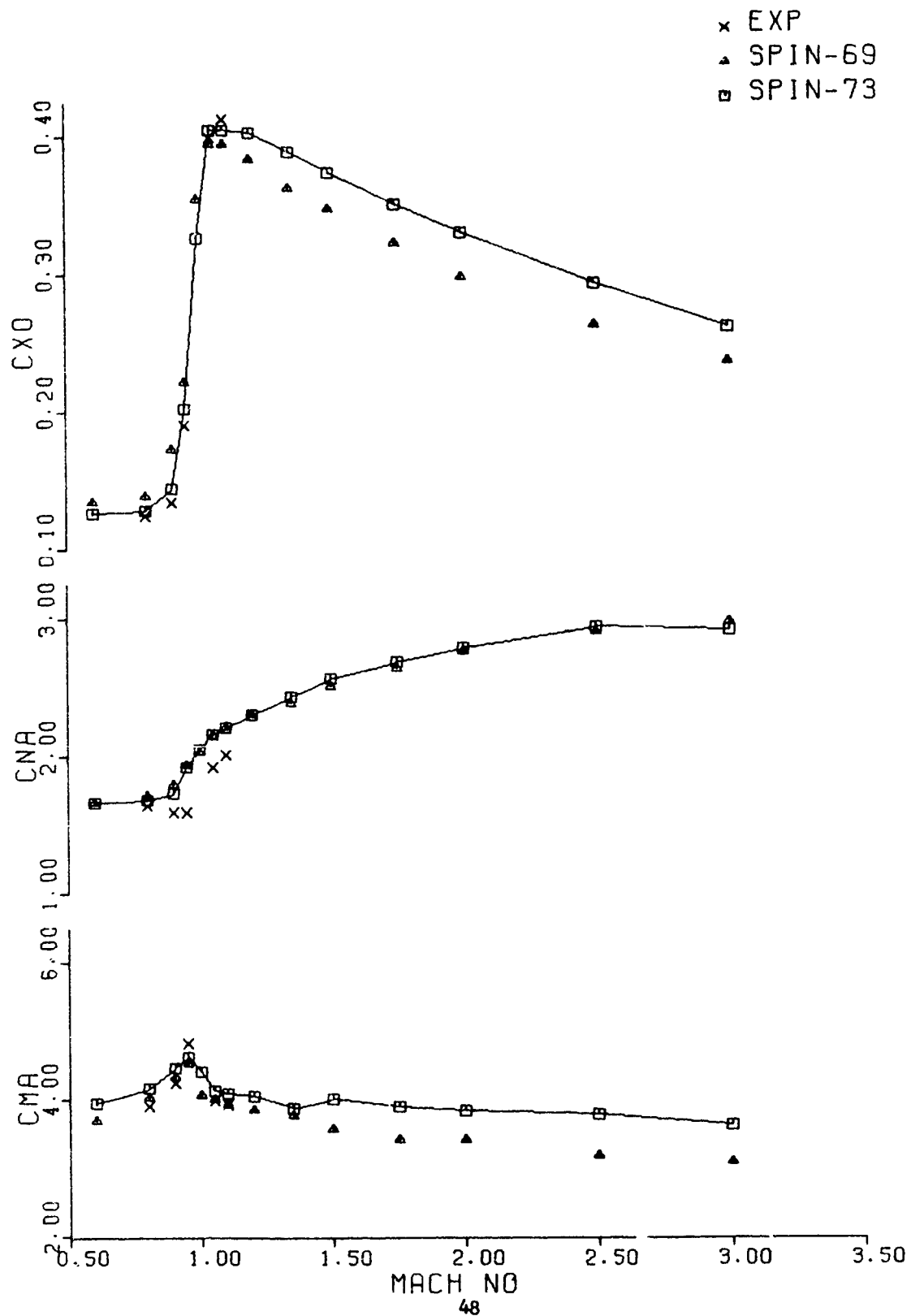


[illegible]

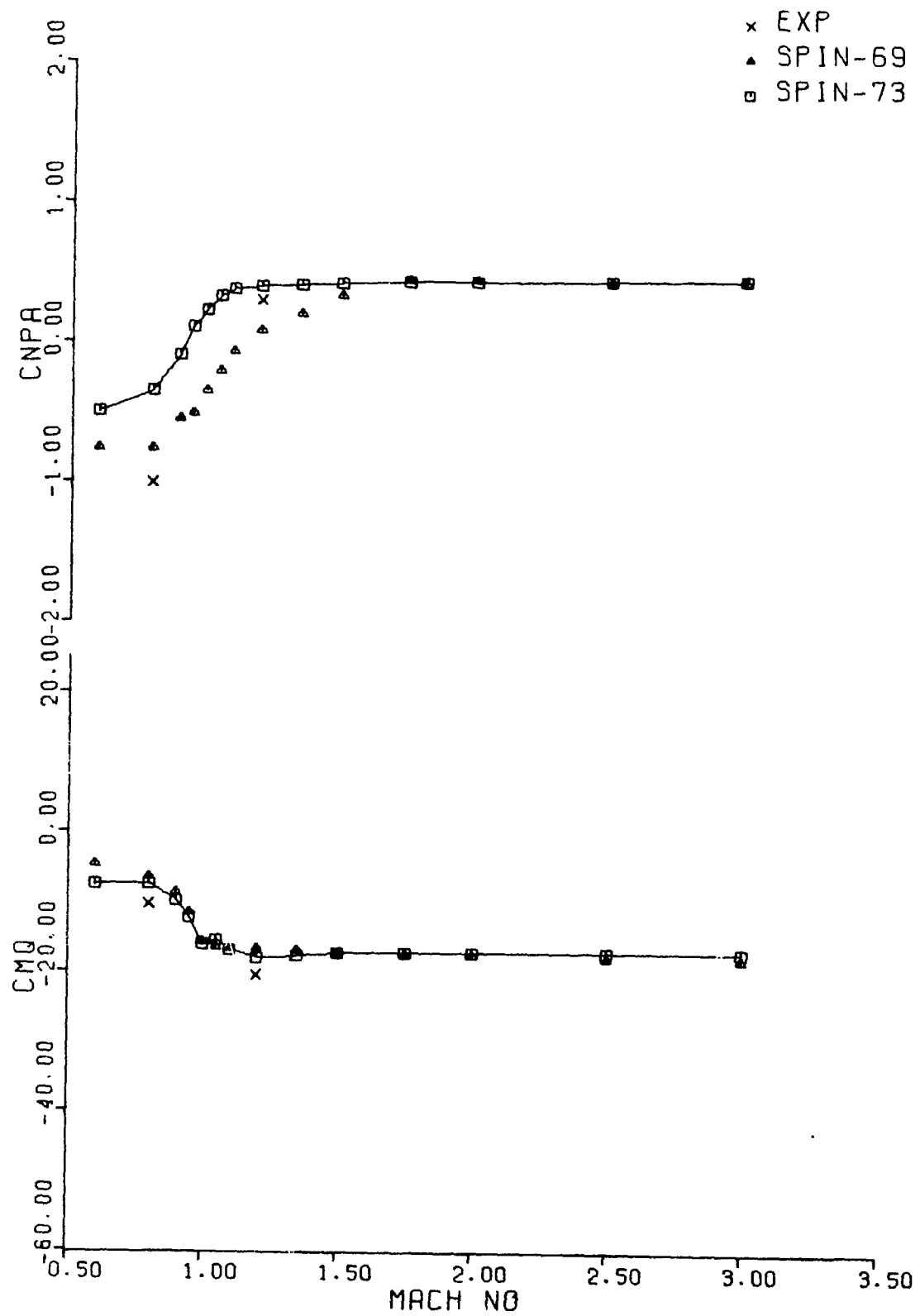
AFRONTIER ENERGY

Best Available Copy

105MM M1



105MM M1



TOTAL		NOSE		BEAT TAIL		CU		MEPLAT		HAND		NOSE		ROOM	
LENGTH	DIAMETER	LENGTH	DIAMETER	LENGTH	DIAMETER	(FM NOSE)	DIAMETER	DIAMETER	DIAMETER	DIAMETER	RADIUS	LENGTH	ROOM	SLUGS/FT ³ X	AIR DENSITY
5.540	0.000	2.900	0.000	0.540	0.000	1.340	0.130	1.023	0.000	10.600	0.00270	0.00270	0.000	0.000	0.000

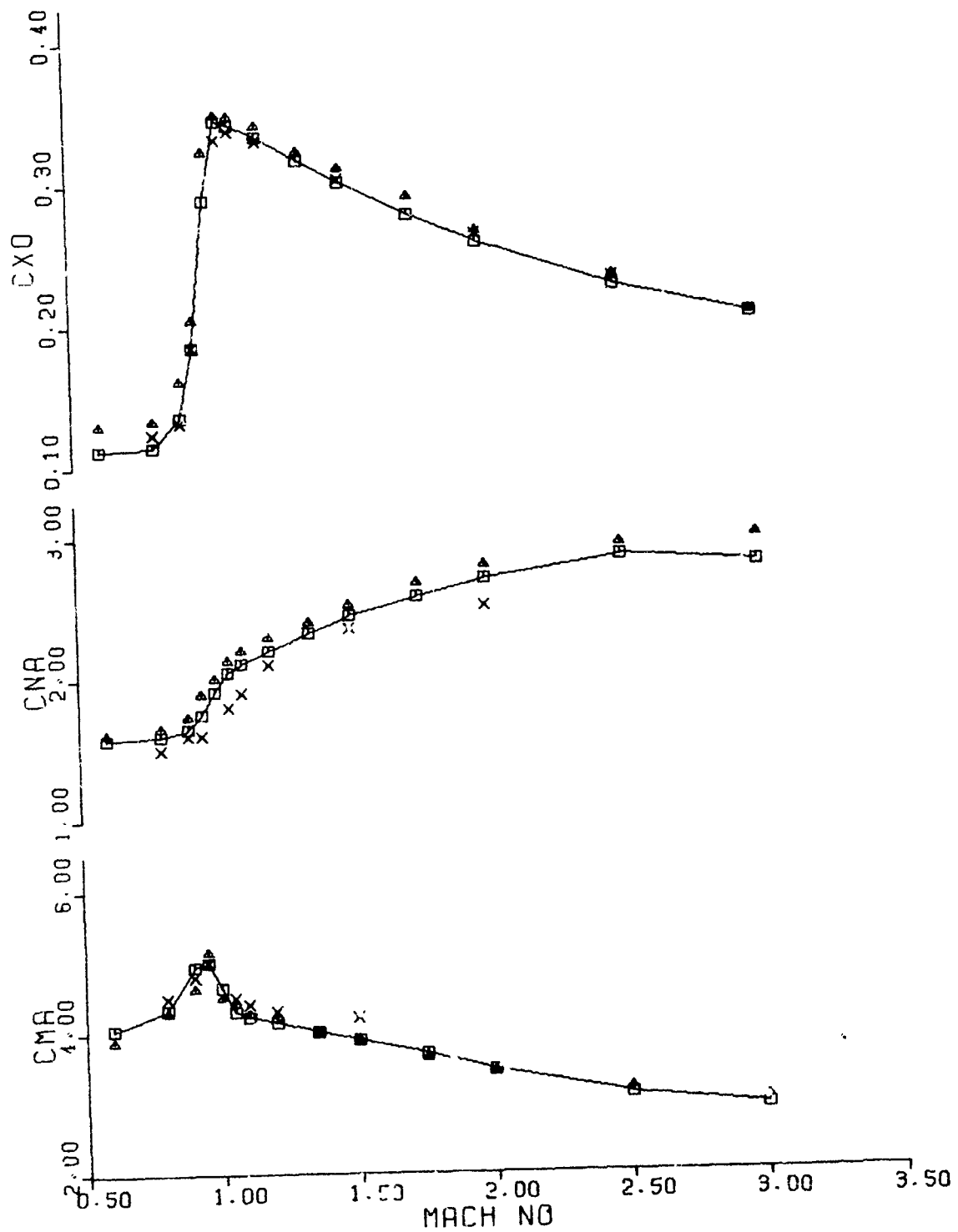
STATISTICAL COEFFICIENTS

WACC	CN	R2	CNA	C42	CGN	CYPA	CNPA	CNPAS	CAPAS	CPFM1	CPFMS	CNPMS	CHQ	CLP
0.013	2.454	1.579	4.045	0.77A	-	-952	-296	108.703	1049.533	3.029	4.061	0.686	-15.510	-0.37
0.013	2.494	1.579	4.070	0.762	-	-952	-316	108.703	1049.533	3.029	4.061	0.686	-15.510	-0.37
0.015	2.065	1.594	4.342	0.730	-	-952	-318	98.783	1049.533	3.217	4.155	0.775	-15.510	-0.35
0.036	3.475	1.647	4.940	0.741	-	-1.043	0.207	72.123	683.733	3.534	4.148	0.859	-17.799	-0.30
0.085	4.936	1.753	4.908	0.48A	-	-1.342	0.509	50.623	524.733	3.719	4.102	1.023	-20.119	-0.26
0.260	4.548	1.913	4.631	0.910	-	-1.231	0.626	38.643	344.933	3.848	4.134	0.977	-23.869	-0.24
0.345	4.644	2.050	4.301	1.242	-	-1.119	0.720	23.143	191.933	3.944	4.175	0.932	-23.251	-0.24
0.342	5.321	2.107	4.220	1.337	-	-1.043	0.759	16.323	128.733	4.054	4.195	0.910	-24.96A	-0.24
0.333	5.913	2.198	4.114	1.450	-	-952	0.757	11.487	77.773	4.136	4.24A	0.865	-26.770	-0.21
0.326	5.356	2.316	3.966	1.615	-	-952	0.755	9.503	57.533	4.155	4.248	0.865	-27.069	-0.23
0.300	4.786	2.443	3.672	1.756	-	-952	0.784	8.511	47.613	4.164	4.248	0.865	-2A.02A	-0.23
0.276	4.221	2.567	3.646	1.904	-	-952	0.793	7.519	37.693	4.173	4.248	0.865	-28.028	-0.23
0.256	3.652	2.695	3.433	2.067	-	-952	0.802	6.527	27.773	4.183	4.248	0.865	-28.028	-0.22
0.224	2.992	2.845	3.075	2.259	-	-952	0.811	5.535	17.653	4.192	4.246	0.865	-28.02A	-0.21
0.203	2.521	2.781	2.891	2.301	-	-952	0.820	4.543	7.933	4.201	4.248	0.865	-28.028	-0.20
0.165	2.086	2.681	2.870	2.370	-	-952	0.820	4.543	7.933	4.201	4.248	0.865	-28.028	-0.20
0.143	1.651	2.581	2.843	2.359	-	-952	0.820	4.543	7.933	4.201	4.248	0.865	-28.028	-0.19

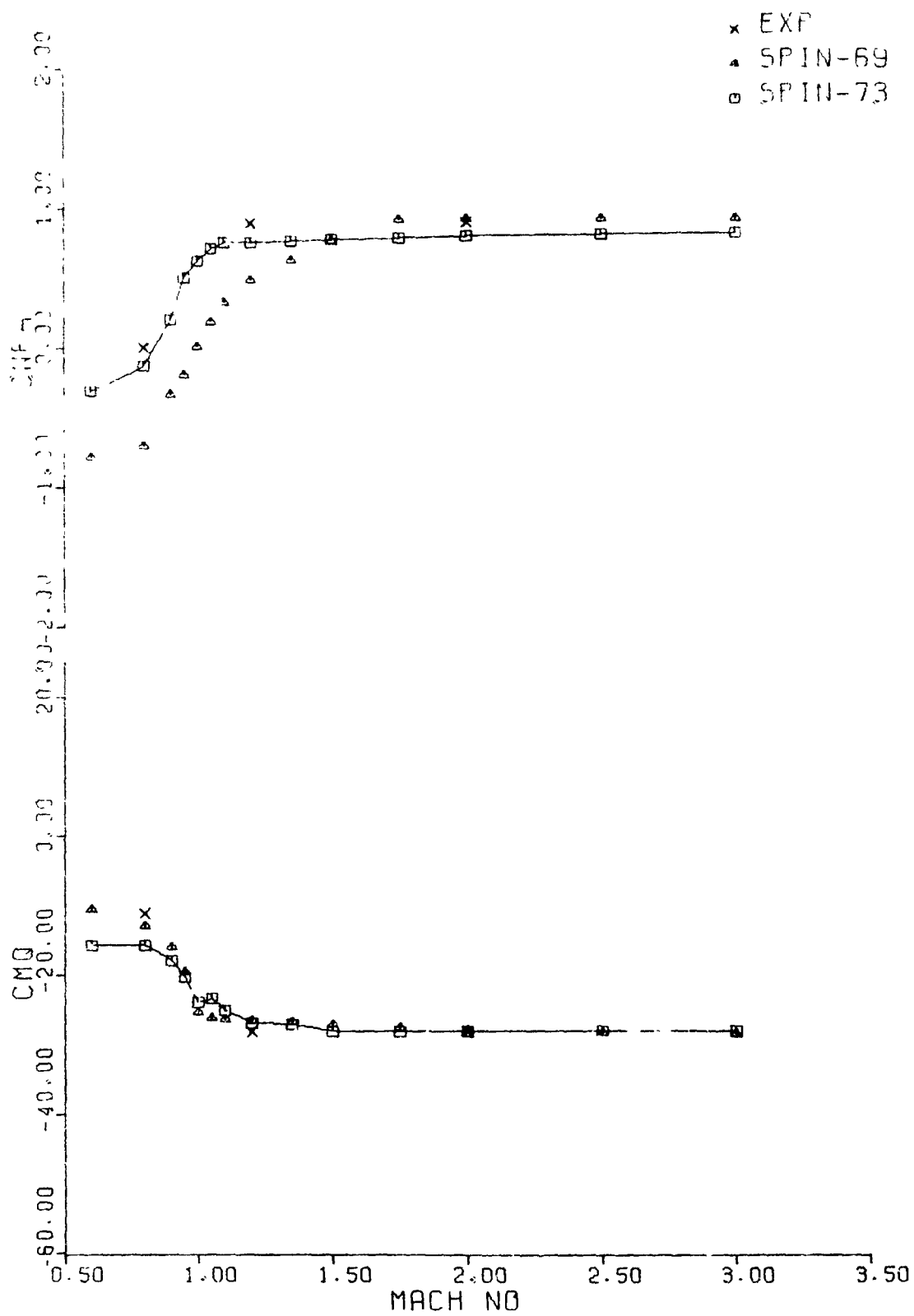
Best Available Copy

105MM XM380E5

x EXP
 ▲ SPIN-69
 □ SPIN-73



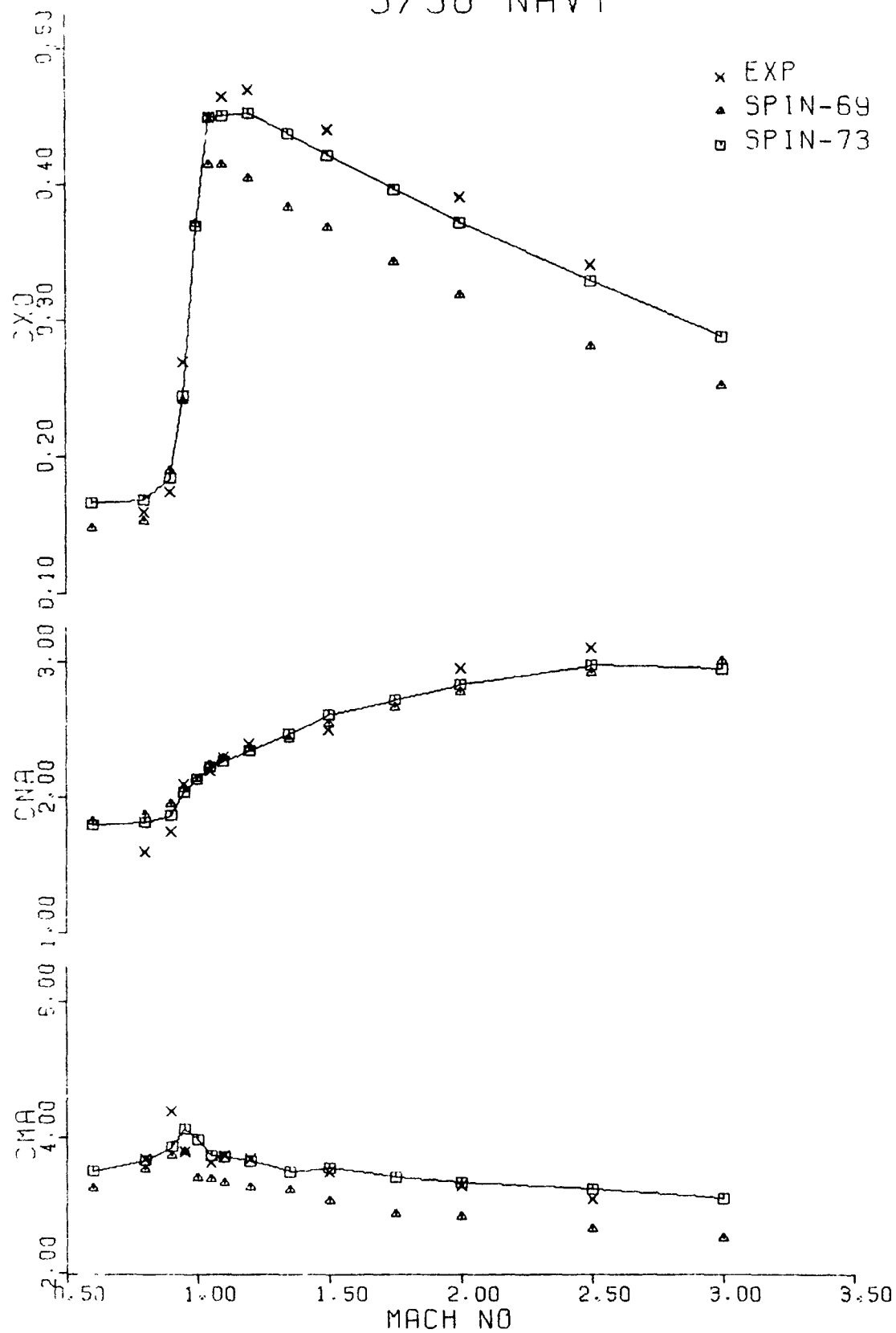
105MM XM380E5



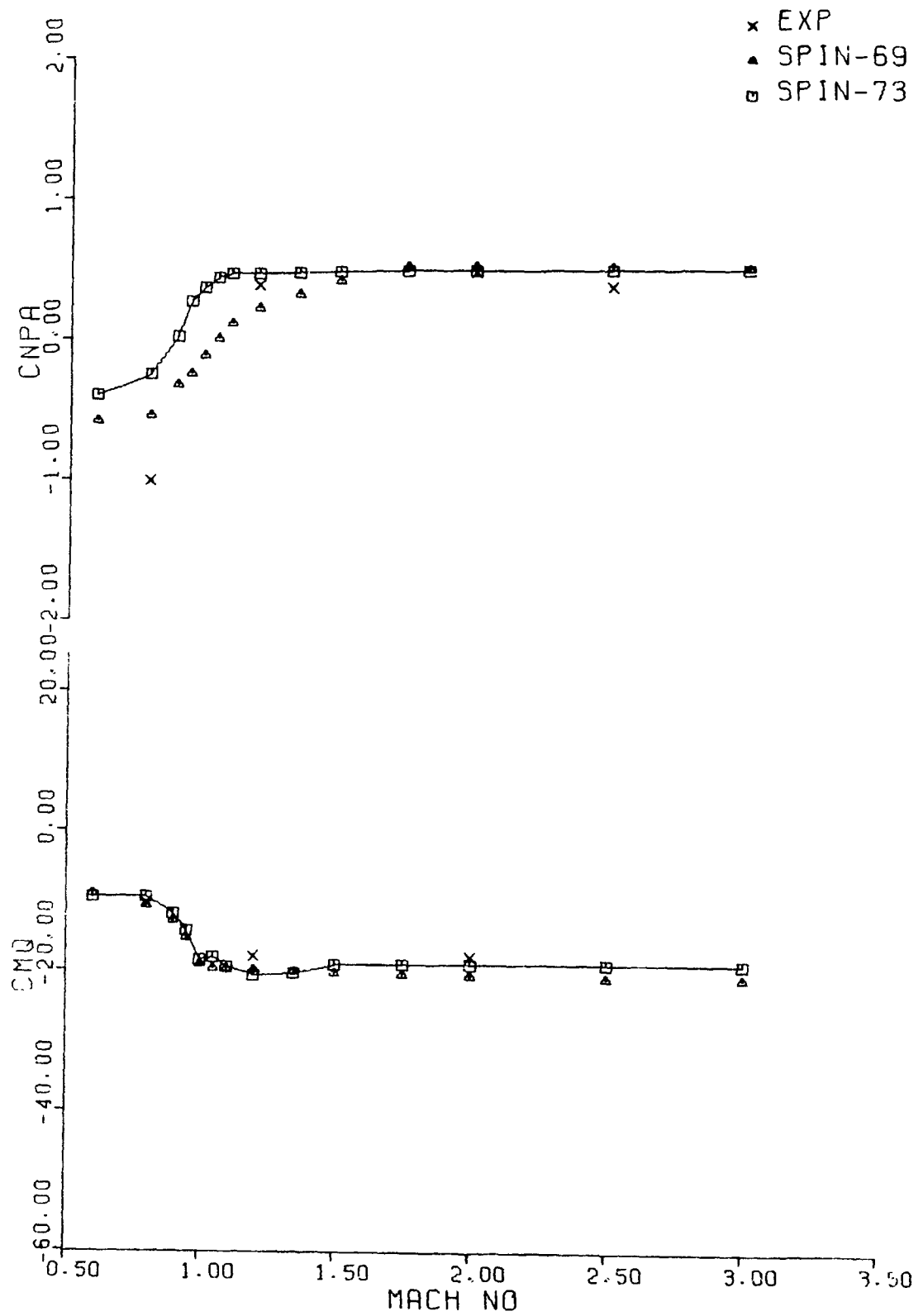
5/34

SCALAR COEFFICIENTS

5/38 NAVY

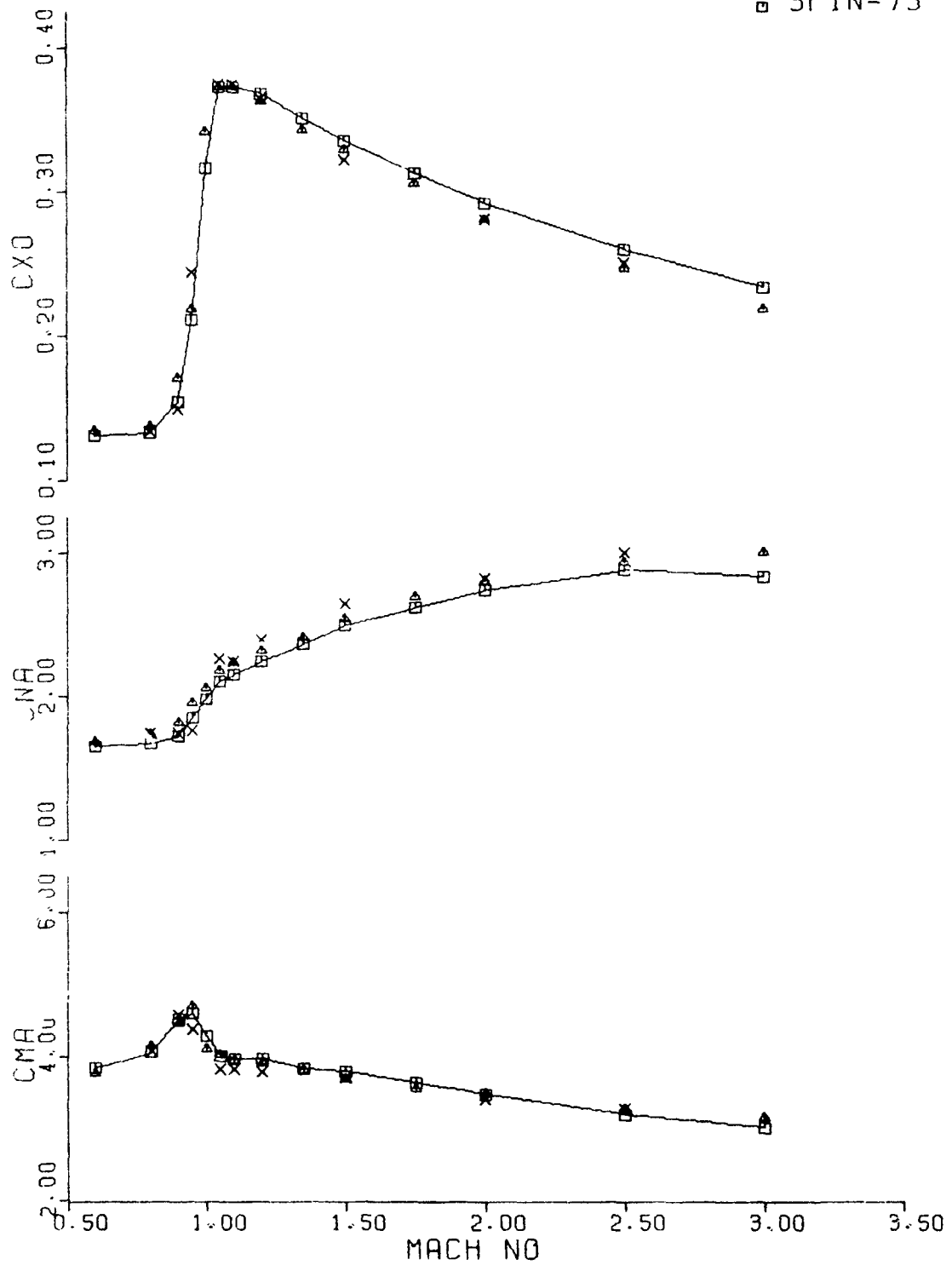


5/38 NAVY

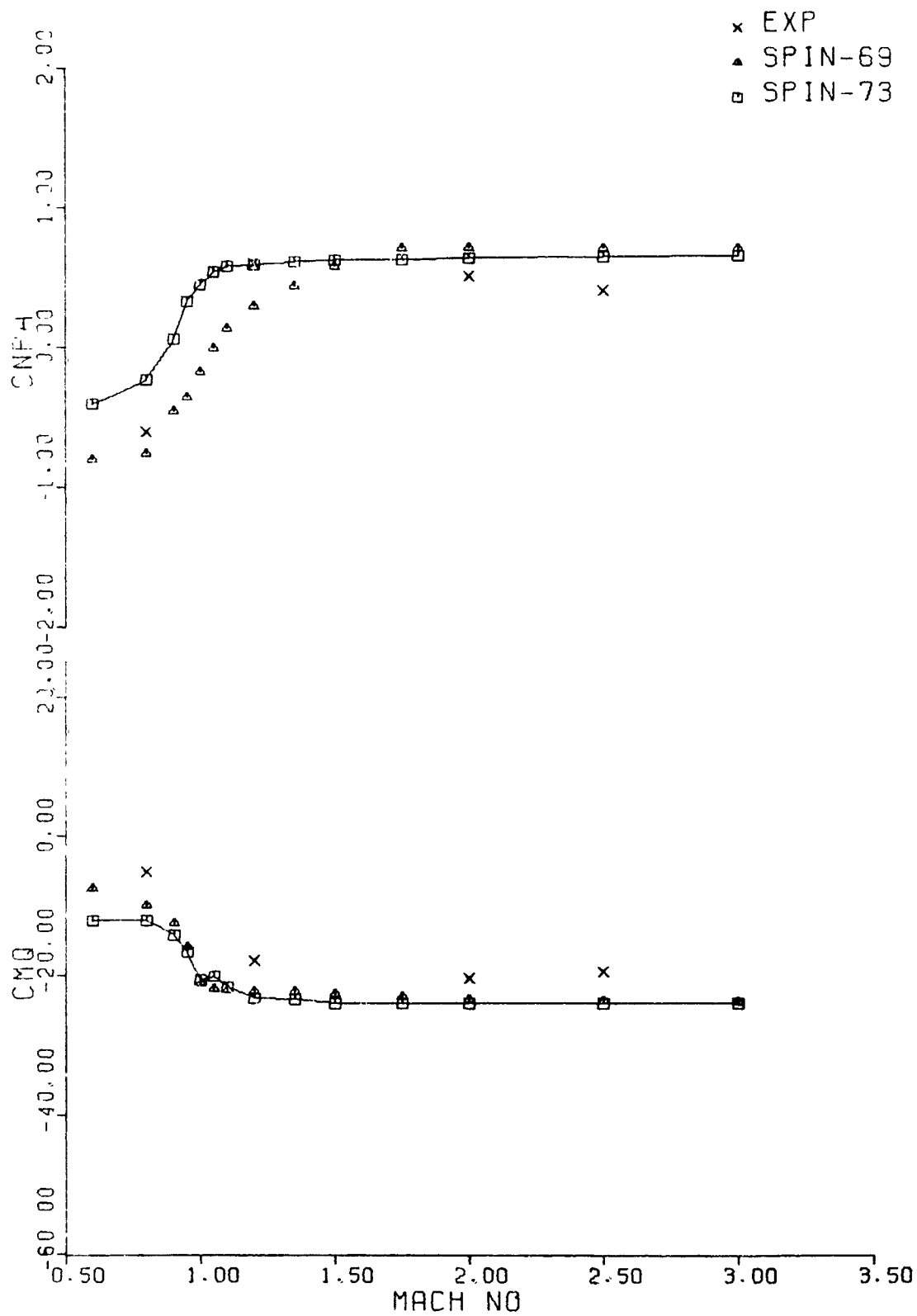


5/54 NAVY

x EXP
 ▲ SPIN-69
 □ SPIN-73



5/54 NAVY



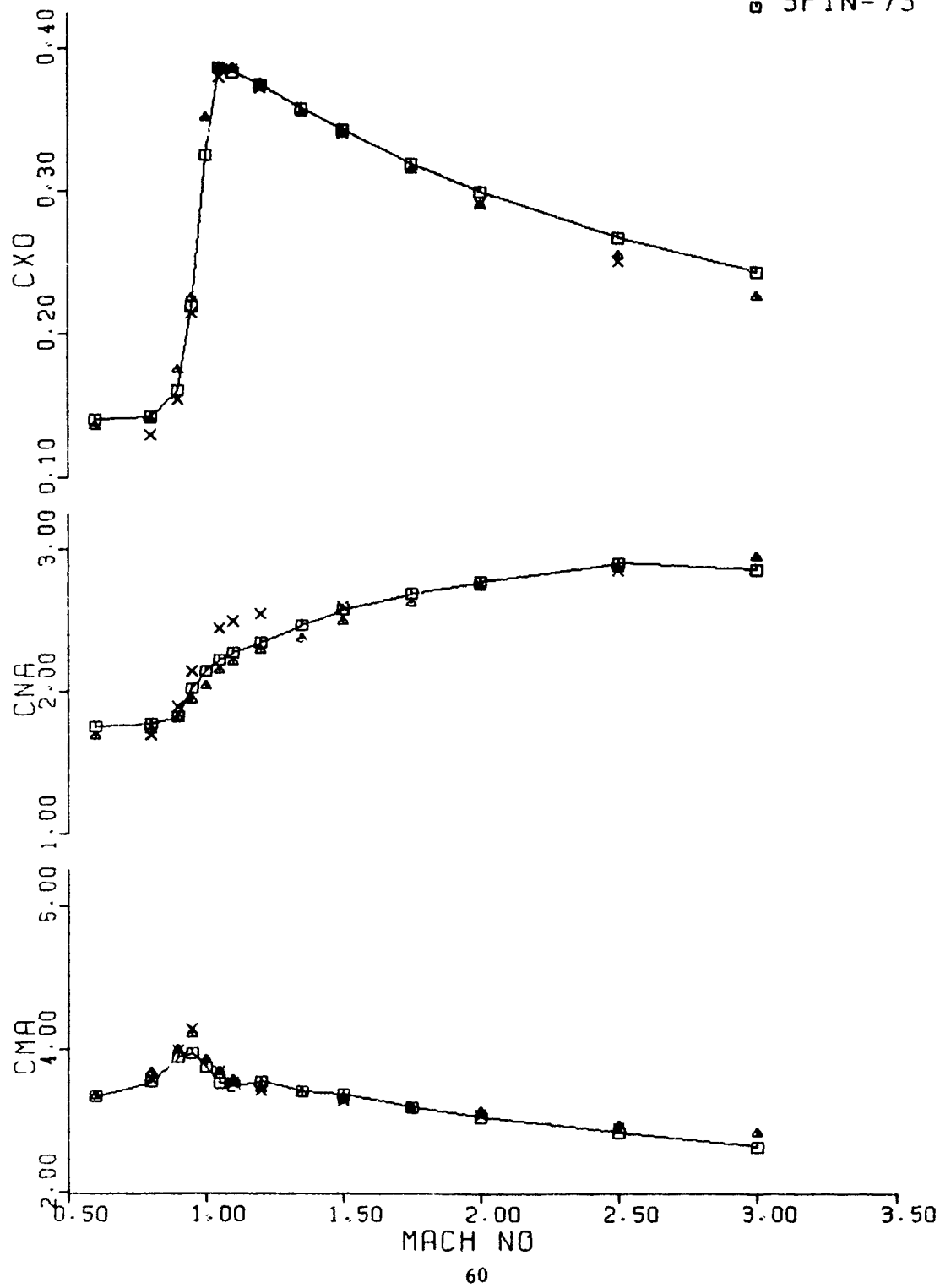
55 M. W. L. INJECTION SYSTEM
-181

DIAMETER INCHES 0.000	IN LB-IN-5 0.1-5	INSE -500TH 5.490	ACT. TAIL LENGTH 0.490	C ₁ (W. NOSE) 2.900	WEPLAT DIAMETER 0.000	MAN DIAMETER 1.020	NOSE RADIUS 10.750	TEMPERATURE DEG-F 0.000	AIR DENSITY G/CM ³ 0.00270	ROOM LENGTH 0.000
HYDRODYNAMIC COEFFICIENTS										
WACH	C ₁	C ₂	C ₃	C ₄	C ₅	C ₆	C ₇	C ₈	C ₉	C ₁₀
0.010	0.001	0.002	0.003	0.004	0.005	0.006	0.007	0.008	0.009	0.010
0.020	0.002	0.004	0.006	0.008	0.010	0.012	0.014	0.016	0.018	0.020
0.030	0.003	0.006	0.009	0.012	0.015	0.018	0.021	0.024	0.027	0.030
0.040	0.004	0.008	0.012	0.016	0.020	0.024	0.028	0.032	0.036	0.040
0.050	0.005	0.010	0.015	0.020	0.025	0.030	0.035	0.040	0.045	0.050
0.060	0.006	0.012	0.018	0.024	0.030	0.036	0.042	0.048	0.054	0.060
0.070	0.007	0.014	0.021	0.028	0.035	0.042	0.049	0.056	0.063	0.070
0.080	0.008	0.016	0.024	0.032	0.040	0.048	0.056	0.064	0.072	0.080
0.090	0.009	0.018	0.027	0.036	0.045	0.054	0.063	0.072	0.081	0.090
0.100	0.010	0.020	0.030	0.040	0.050	0.060	0.070	0.080	0.090	0.100
0.120	0.012	0.024	0.036	0.048	0.060	0.072	0.084	0.096	0.108	0.120
0.140	0.014	0.028	0.042	0.056	0.070	0.084	0.098	0.112	0.126	0.140
0.160	0.016	0.032	0.048	0.064	0.080	0.096	0.112	0.128	0.144	0.160
0.180	0.018	0.036	0.054	0.072	0.090	0.108	0.126	0.144	0.162	0.180
0.200	0.020	0.040	0.060	0.080	0.100	0.120	0.140	0.160	0.180	0.200
0.250	0.025	0.050	0.075	0.100	0.125	0.150	0.175	0.200	0.225	0.250
0.300	0.030	0.060	0.090	0.120	0.150	0.180	0.210	0.240	0.270	0.300
0.350	0.035	0.070	0.105	0.140	0.175	0.210	0.245	0.280	0.315	0.350
0.400	0.040	0.080	0.120	0.160	0.200	0.240	0.280	0.320	0.360	0.400
0.450	0.045	0.090	0.135	0.180	0.225	0.270	0.315	0.360	0.405	0.450
0.500	0.050	0.100	0.150	0.200	0.250	0.300	0.350	0.400	0.450	0.500

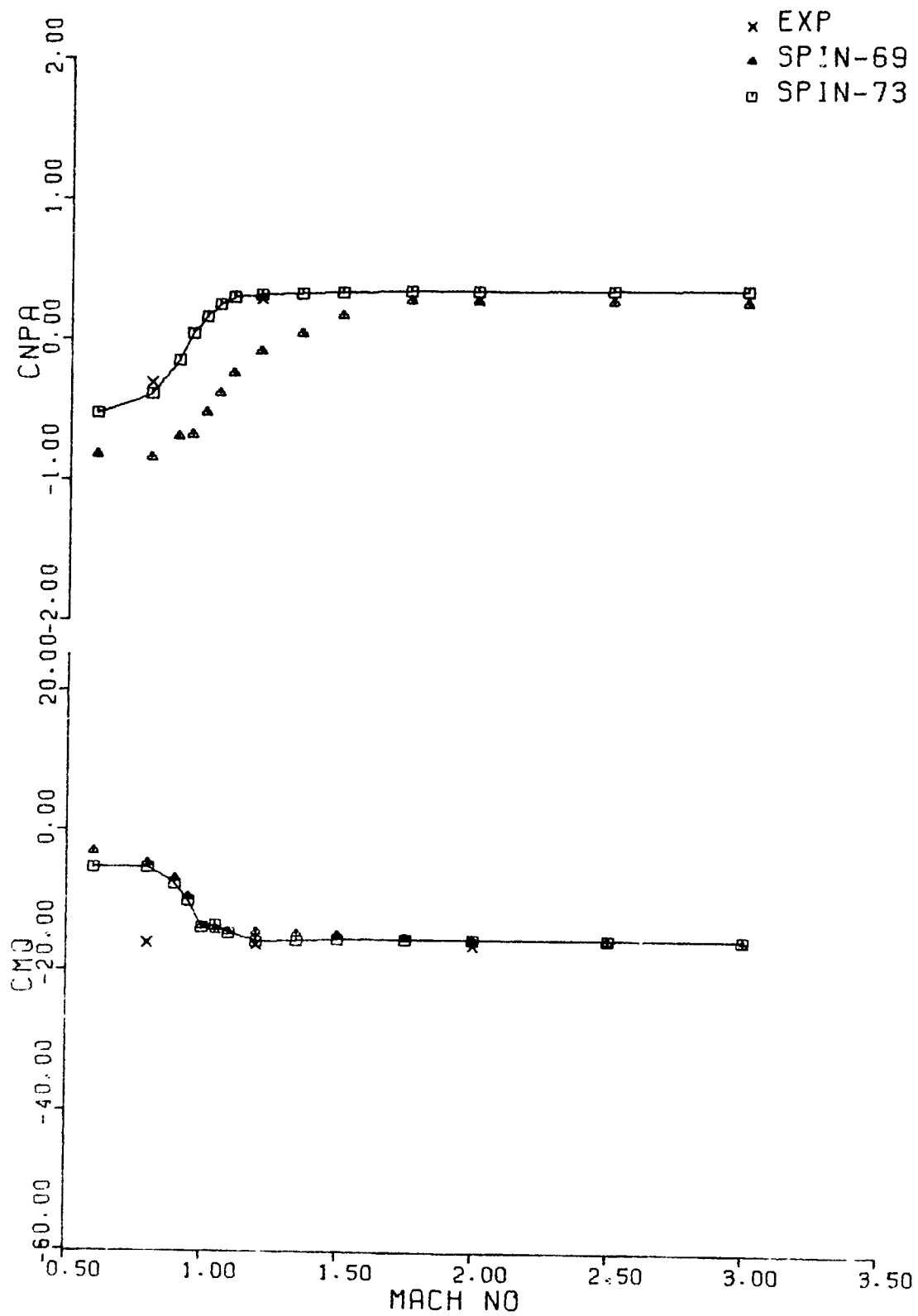
Best Available Copy

155MM M101/107

x EXP
 ▲ SPIN-69
 □ SPIN-73

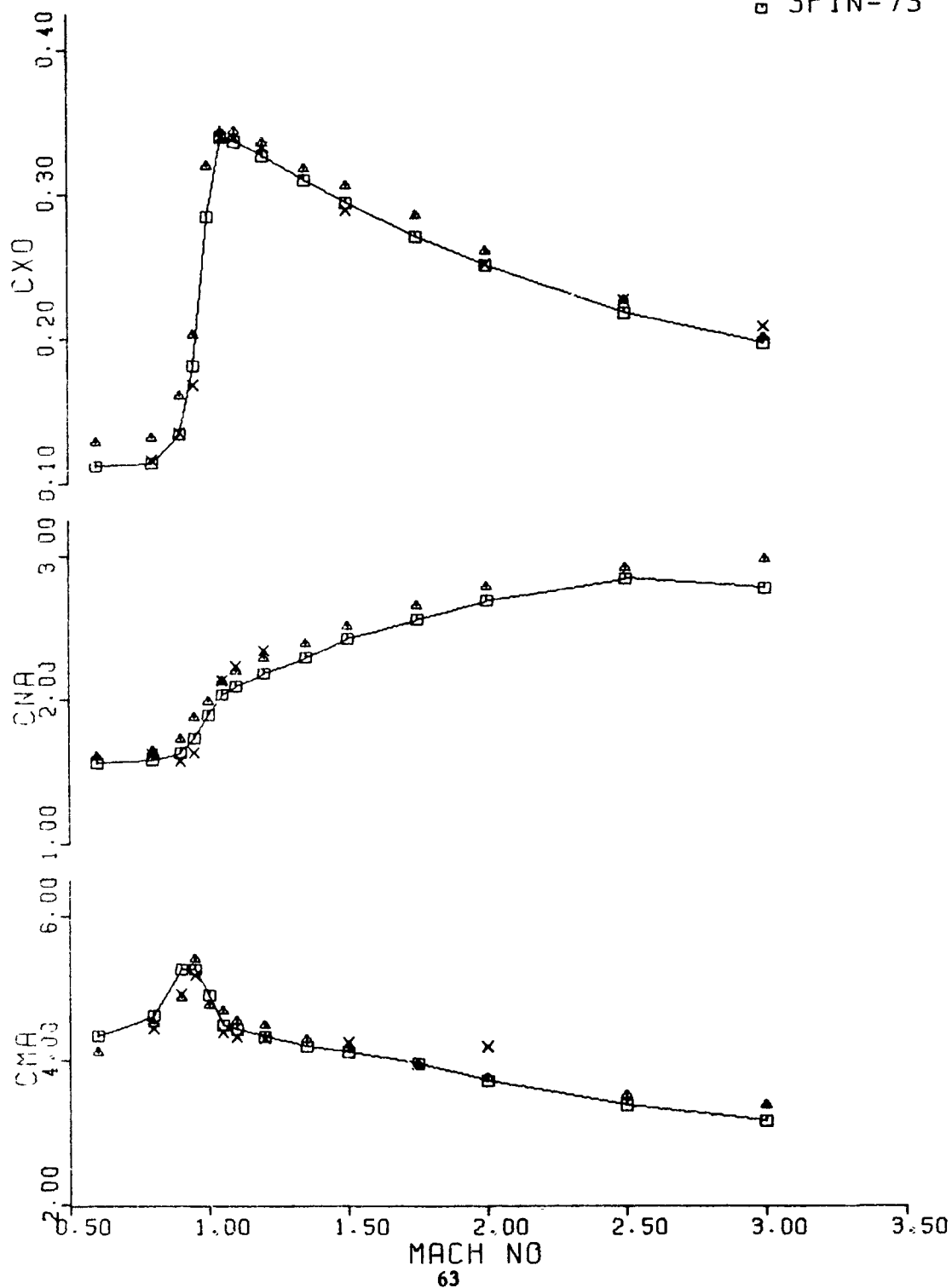


155MM M101/107

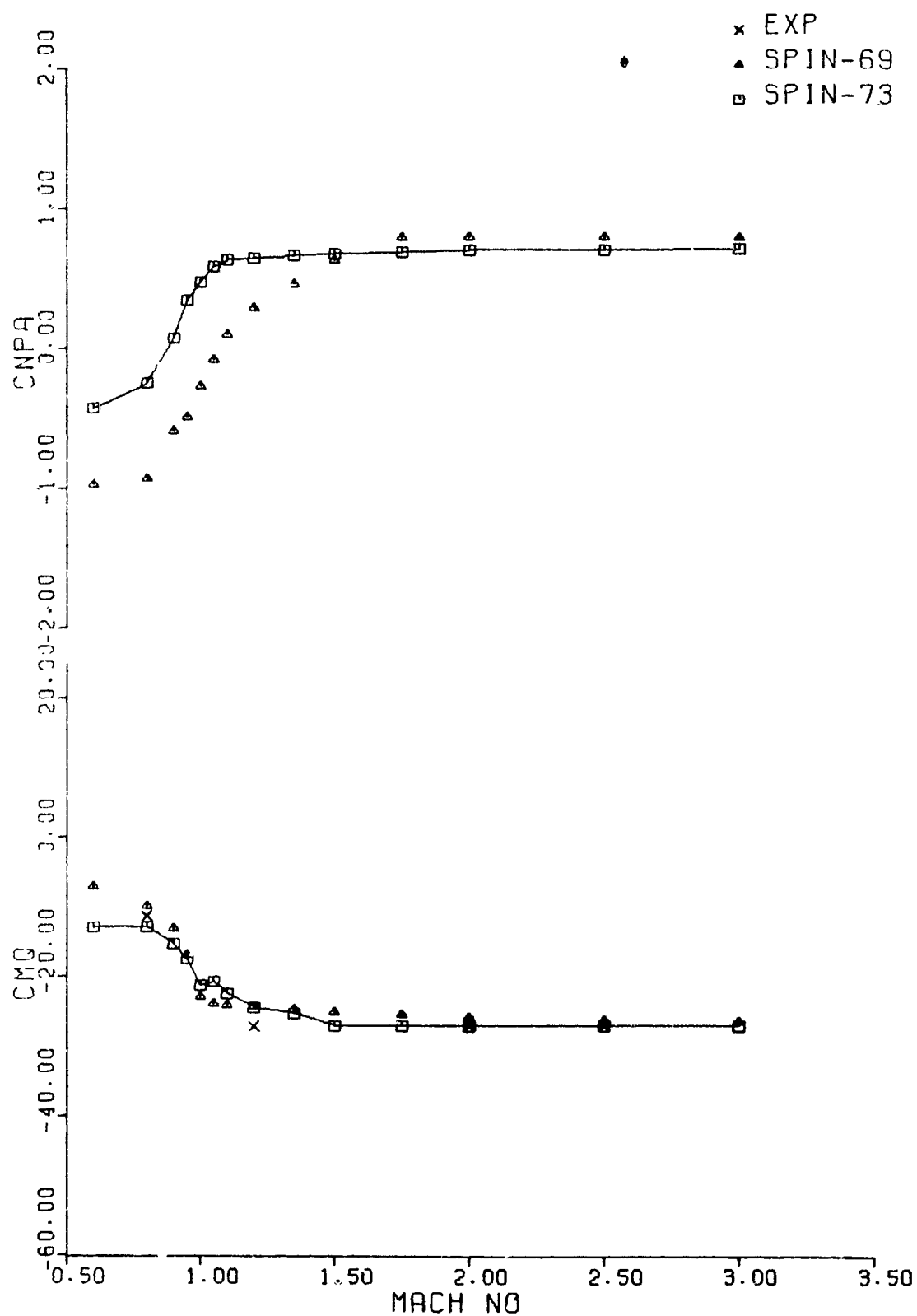


155MM M549

- x EXP
- ▲ SPIN-69
- SPIN-73



155MM M549



TOTAL LENGTH 5.510

BEAT TAIL
-EAGLE
1.000

(E)

2000

1979

070
0105
350

FROM
FIGHT
END

SEP 17
SHEILA
W-3-71

500

75-1000
A

500
55
44

7.10.
7.11.
7.12.

—

500
SES
7404

100-3-6
100-3-6

5177
7002
16

2. 4. 21 23 25 27 29 31 33 35 37 39 41 43 45 47 49 51 53 55 57 59 61 63 65 67 69 71 73 75 77 79 81 83 85 87 89 91 93 95 97 99 101 103 105 107 109 111 113 115 117 119 121 123 125 127 129 131 133 135 137 139 141 143 145 147 149 151 153 155 157 159 161 163 165 167 169 171 173 175 177 179 181 183 185 187 189 191 193 195 197 199 201 203 205 207 209 211 213 215 217 219 221 223 225 227 229 231 233 235 237 239 241 243 245 247 249 251 253 255 257 259 261 263 265 267 269 271 273 275 277 279 281 283 285 287 289 291 293 295 297 299 301 303 305 307 309 311 313 315 317 319 321 323 325 327 329 331 333 335 337 339 341 343 345 347 349 351 353 355 357 359 361 363 365 367 369 371 373 375 377 379 381 383 385 387 389 391 393 395 397 399 401 403 405 407 409 411 413 415 417 419 421 423 425 427 429 431 433 435 437 439 441 443 445 447 449 451 453 455 457 459 461 463 465 467 469 471 473 475 477 479 481 483 485 487 489 491 493 495 497 499 501 503 505 507 509 511 513 515 517 519 521 523 525 527 529 531 533 535 537 539 541 543 545 547 549 551 553 555 557 559 561 563 565 567 569 571 573 575 577 579 581 583 585 587 589 591 593 595 597 599 601 603 605 607 609 611 613 615 617 619 621 623 625 627 629 631 633 635 637 639 641 643 645 647 649 651 653 655 657 659 661 663 665 667 669 671 673 675 677 679 681 683 685 687 689 691 693 695 697 699 701 703 705 707 709 711 713 715 717 719 721 723 725 727 729 731 733 735 737 739 741 743 745 747 749 751 753 755 757 759 761 763 765 767 769 771 773 775 777 779 781 783 785 787 789 791 793 795 797 799 801 803 805 807 809 811 813 815 817 819 821 823 825 827 829 831 833 835 837 839 841 843 845 847 849 851 853 855 857 859 861 863 865 867 869 871 873 875 877 879 881 883 885 887 889 891 893 895 897 899 901 903 905 907 909 911 913 915 917 919 921 923 925 927 929 931 933 935 937 939 941 943 945 947 949 951 953 955 957 959 961 963 965 967 969 971 973 975 977 979 981 983 985 987 989 991 993 995 997 999 1001 1003 1005 1007 1009 1011 1013 1015 1017 1019 1021 1023 1025 1027 1029 1031 1033 1035 1037 1039 1041 1043 1045 1047 1049 1051 1053 1055 1057 1059 1061 1063 1065 1067 1069 1071 1073 1075 1077 1079 1081 1083 1085 1087 1089 1091 1093 1095 1097 1099 1101 1103 1105 1107 1109 1111 1113 1115 1117 1119 1121 1123 1125 1127 1129 1131 1133 1135 1137 1139 1141 1143 1145 1147 1149 1151 1153 1155 1157 1159 1161 1163 1165 1167 1169 1171 1173 1175 1177 1179 1181 1183 1185 1187 1189 1191 1193 1195 1197 1199 1201 1203 1205 1207 1209 1211 1213 1215 1217 1219 1221 1223 1225 1227 1229 1231 1233 1235 1237 1239 1241 1243 1245 1247 1249 1251 1253 1255 1257 1259 1261 1263 1265 1267 1269 1271 1273 1275 1277 1279 1281 1283 1285 1287 1289 1291 1293 1295 1297 1299 1301 1303 1305 1307 1309 1311 1313 1315 1317 1319 1321 1323 1325 1327 1329 1331 1333 1335 1337 1339 1341 1343 1345 1347 1349 1351 1353 1355 1357 1359 1361 1363 1365 1367 1369 1371 1373 1375 1377 1379 1381 1383 1385 1387 1389 1391 1393 1395 1397 1399 1401 1403 1405 1407 1409 1411 1413 1415 1417 1419 1421 1423 1425 1427 1429 1431 1433 1435 1437 1439 1441 1443 1445 1447 1449 1451 1453 1455 1457 1459 1461 1463 1465 1467 1469 1471 1473 1475 1477 1479 1481 1483 1485 1487 1489 1491 1493 1495 1497 1499 1501 1503 1505 1507 1509 1511 1513 1515 1517 1519 1521 1523 1525 1527 1529 1531 1533 1535 1537 1539 1541 1543 1545 1547 1549 1551 1553 1555 1557 1559 1561 1563 1565 1567 1569 1571 1573 1575 1577 1579 1581 1583 1585 1587 1589 1591 1593 1595 1597 1599 1601 1603 1605 1607 1609 1611 1613 1615 1617 1619 1621 1623 1625 1627 1629 1631 1633 1635 1637 1639 1641 1643 1645 1647 1649 1651 1653 1655 1657 1659 1661 1663 1665 1667 1669 1671 1673 1675 1677 1679 1681 1683 1685 1687 1689 1691 1693 1695 1697 1699 1701 1703 1705 1707 1709 1711 1713 1715 1717 1719 1721 1723 1725 1727 1729 1731 1733 1735 1737 1739 1741 1743 1745 1747 1749 1751 1753 1755 1757 1759 1761 1763 1765 1767 1769 1771 1773 1775 1777 1779 1781 1783 1785 1787 1789 1791 1793 1795 1797 1799 1801 1803 1805 1807 1809 1811 1813 1815 1817 1819 1821 1823 1825 1827 1829 1831 1833 1835 1837 1839 1841 1843 1845 1847 1849 1851 1853 1855 1857 1859 1861 1863 1865 186

[illegible]

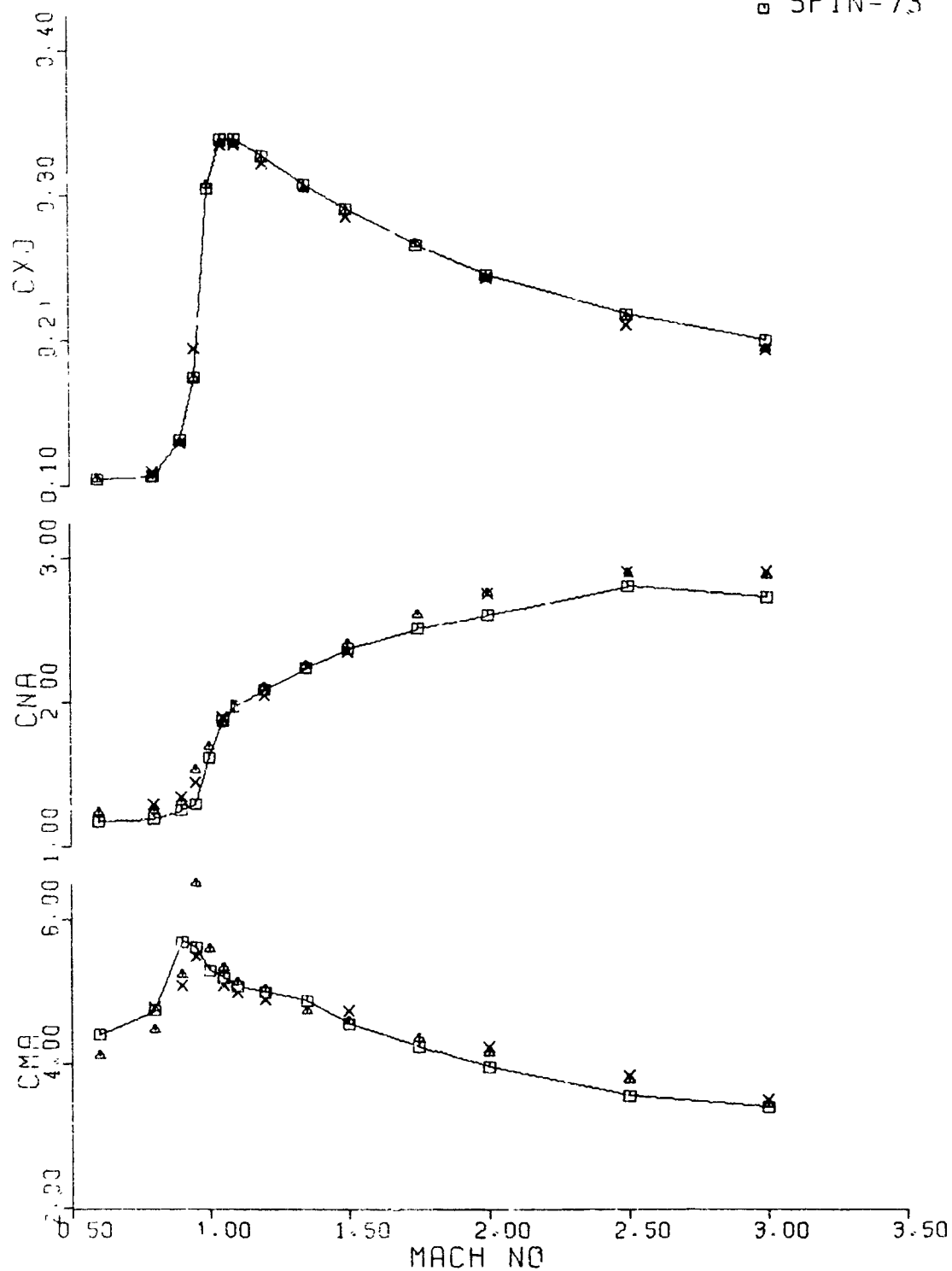
STABILITY ANALYSIS

UYN0	SNAR	RECIP	SHAR5	RECIP5	SPIN	W1	W2	U	L2	U15	L25	DEL	D15P
1.760	-0.721	-6.798	1.399	1.189	6.1	0.45	0.09	-0.00445	0.000096	-0.00073	-0.00267	0.7749	0.330
1.749	-0.701	-6.798	1.399	1.189	366.9	26.69	5.57	-0.00445	0.000097	-0.00073	-0.00267	0.7749	0.330
1.749	-0.701	-6.798	1.399	1.189	469.2	36.70	8.22	-0.00445	0.000097	-0.00073	-0.00267	0.7749	0.330
1.618	2.747	2.747	1.532	1.395	550.9	16.53	11.45	-0.00349	-0.00035	-0.00039	-0.00345	0.0084	0.263
1.559	0.559	0.900	1.320	1.214	550.9	16.53	11.45	-0.00349	-0.00035	-0.00039	-0.00345	0.0084	0.263
1.373	0.713	1.086	1.326	1.119	550.9	16.53	11.45	-0.00349	-0.00035	-0.00039	-0.00345	0.0084	0.263
1.453	0.814	1.036	1.362	1.027	511.5	41.89	11.87	-0.00327	-0.00109	-0.00081	-0.00347	0.0061	0.194
1.480	1.039	1.001	1.253	1.066	642.1	44.37	12.09	-0.00223	-0.00245	-0.00135	-0.00375	0.0075	0.258
1.516	1.097	1.003	1.200	1.042	722.6	46.42	12.32	-0.00141	-0.00310	-0.00164	-0.00375	0.0075	0.316
1.546	1.096	1.003	1.150	1.023	733.8	51.43	13.09	-0.00129	-0.00328	-0.00205	-0.00371	0.0061	0.351
1.629	1.121	1.015	1.201	1.042	825.5	48.26	14.32	-0.00219	-0.00353	-0.00183	-0.00349	0.0054	0.442
1.690	1.132	1.018	1.201	1.042	937.2	46.09	14.56	-0.00224	-0.00362	-0.00194	-0.00349	0.0048	0.542
1.823	1.154	1.025	1.216	1.049	1070.1	78.66	15.43	-0.00222	-0.00373	-0.00197	-0.00359	0.0040	0.663
1.945	1.174	1.031	1.256	1.054	1253.0	91.25	16.28	-0.00221	-0.00381	-0.00199	-0.00403	0.0034	0.772
2.167	1.202	1.042	1.245	1.064	1528.7	116.48	17.93	-0.00219	-0.00396	-0.00202	-0.00413	0.0027	0.949
2.269	1.203	1.043	1.240	1.061	1834.4	140.96	20.33	-0.00219	-0.00391	-0.00204	-0.00405	0.0022	1.035
2.289	1.197	1.040	1.234	1.058	2445.9	188.22	26.84	-0.00220	-0.00393	-0.00206	-0.00397	0.0017	1.020
2.313	1.189	1.037	1.227	1.054	3057.4	235.69	33.14	-0.00222	-0.00375	-0.00207	-0.00389	0.0013	1.001

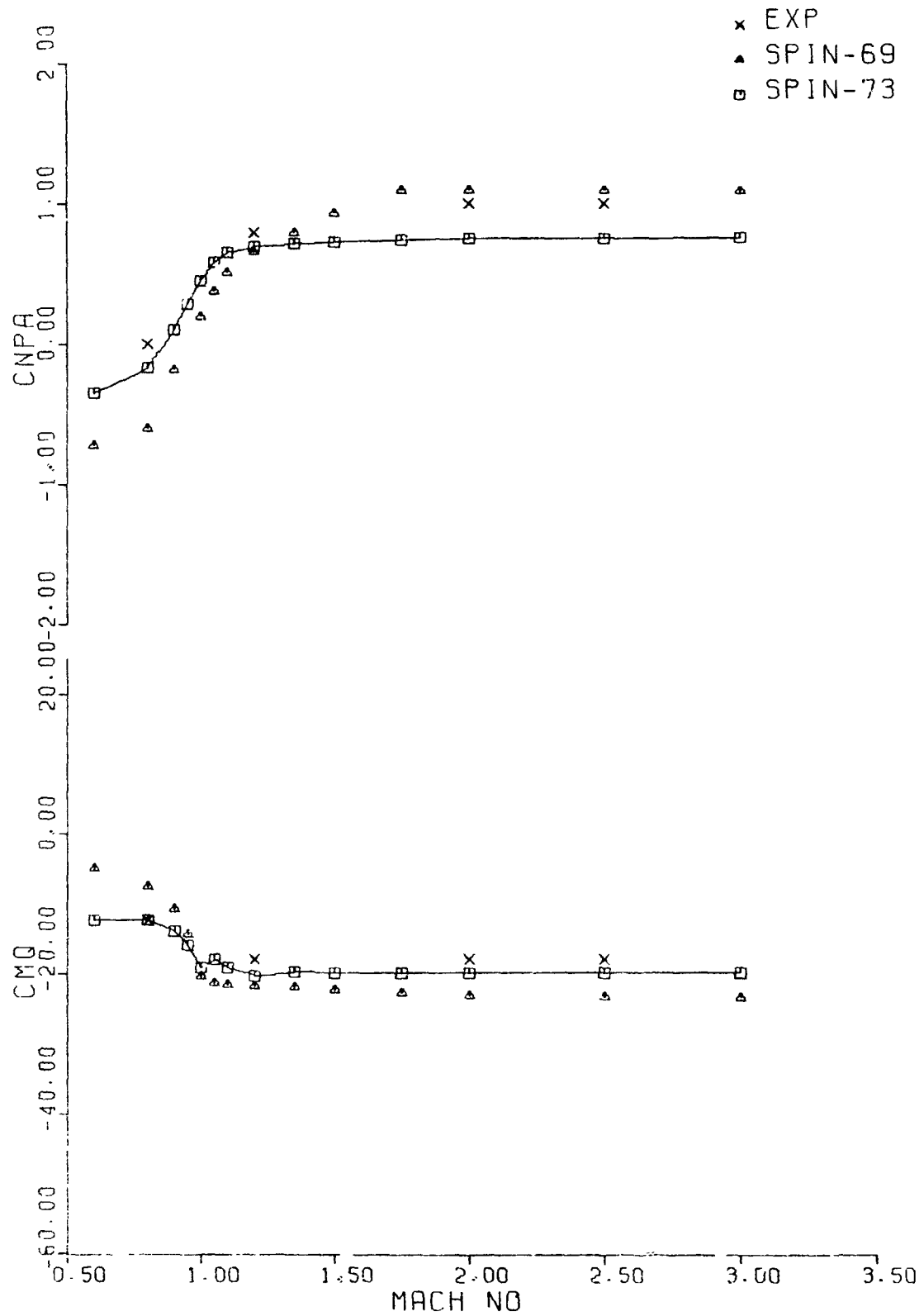
Best Available Copy

175MM M437

x EXP
 ▲ SPIN-69
 □ SPIN-73



175MM M437

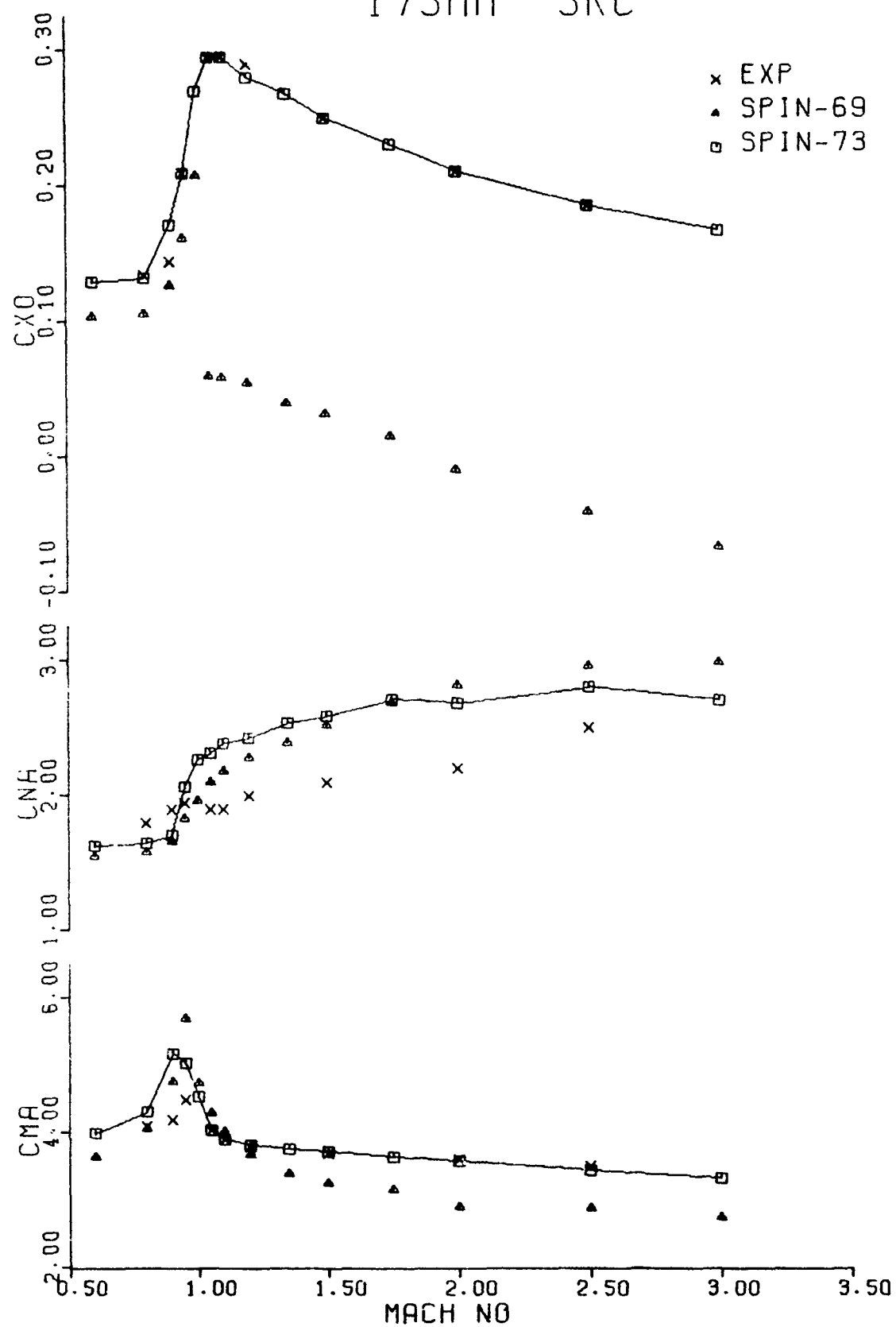


[illegible]

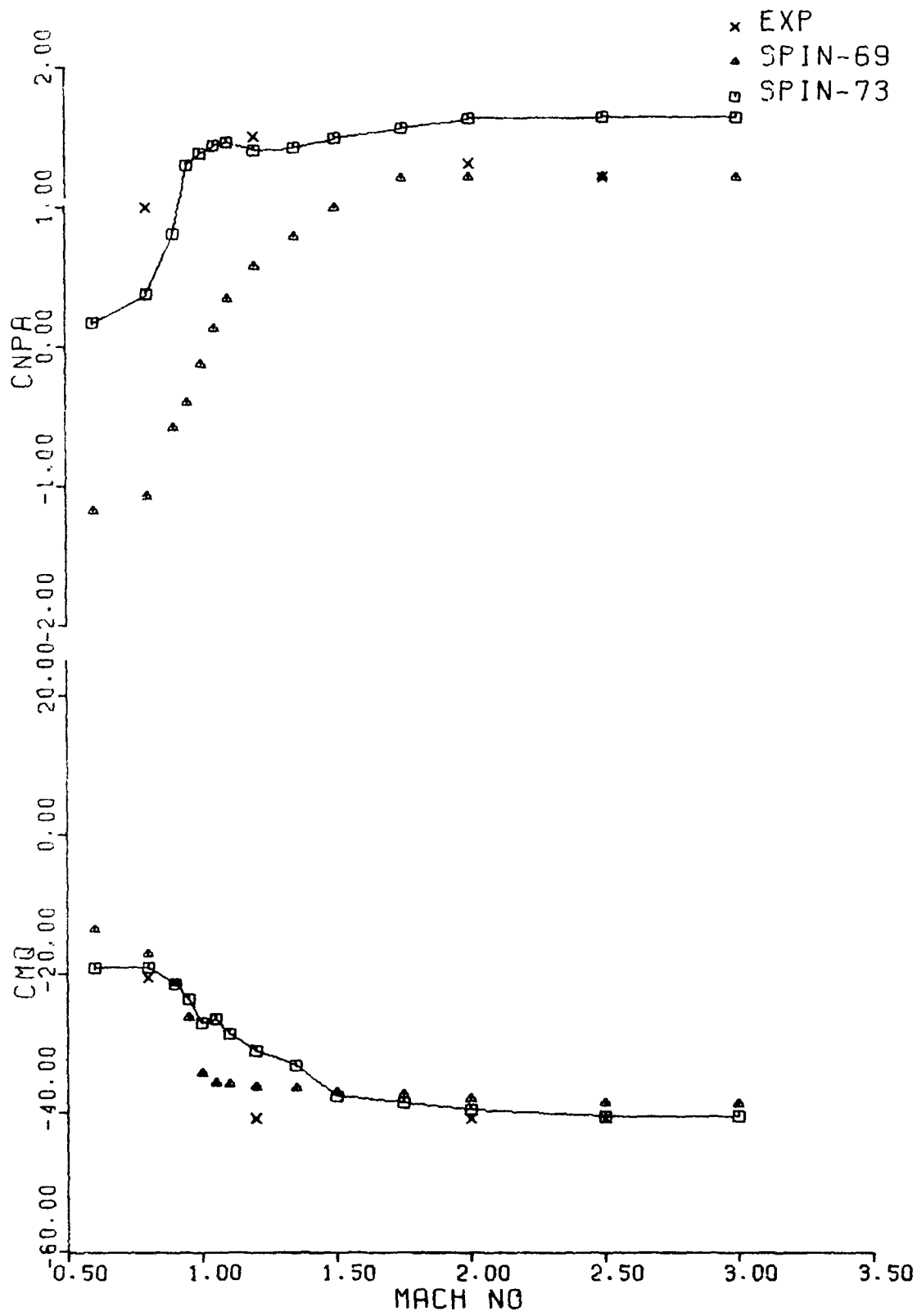
ANALYTICAL CHEMISTRY, 15

Best Available Copy

175MM SRC



175MM SRC



APPENDIX A

CURVE FIT TECHNIQUE

CURVE FIT TECHNIQUE

The method used to perform least squares fits to the experimental data using the empirical equations was a GE Time Sharing computer program code name LSQMM. This program was utilized with the GE415 computer at the Armament Systems Department. The brief description starting on the next page of this program was extracted from the following reference.

Numerical Analysis Routines #807231A
Information Service Department
General Electric Company
Bethesda, Maryland

Issued August 1968 (Revised Feb. 1969)

LSQMM

This routine determines the coefficients $A(J), J=1,2,\dots,N$ of the function

$$F(I) = A_1 Q_{I,1} + A_2 Q_{I,2} + \dots + A_N Q_{I,N} \quad I = 1,2,\dots,M$$

which determines the best approximation of the function $Y(I)$ in either the weighted least squares sense or the min-max sense.

Usage

The calling sequence for this routine is:

CALL LSQMM(PHI,Y,A,RW,M,N,NT,NS,AM,IDIMM,IDIMN)

where,

- PHI is the two dimensional array, PHI(M,N), of coordinate functions which are supplied by the user. The k^{th} column of PHI contains the k^{th} coordinate function evaluated at each of the data points (i.e., $\text{PHI}(I,k), I = 1,2,\dots,M$).
- Y is the one dimensional array, Y(M), containing the dependent variables.
- A is the one dimensional array, A(N).
- The A array contains the coefficients $A(J)$ of the function $F(I)$.
- RW is the name of an array containing the residuals $R(I) = Y(I) - F(I)$, the weights $W(I)$, and temporary storage to save the vertical weights while doing the horizontal iterations. It should contain at least $3 \cdot M$ locations.
- M is the number of data points.
- N is the number of coefficients, i.e., number of coordinate functions.
- NT is the maximum number of vertical iterations. For least squares fit, $NT = 1$.
- For least squares fit and when there is no division of the data points in min-max, $NS(1) = M$. Otherwise, NS is the array containing the index values of the ends of the sections when using min-max fit.
- AM is a two dimensional array, AM(N,N), used internally to contain the matrix of the system of linear equations.
- IDIMM is the first dimension of PHI, i.e., $\text{PHI}(\text{IDIMM},N)$.
- IDIMN is the first dimension of AM, i.e., $\text{AM}(\text{IDIMN},N)$.

Discussion

If the user wishes to minimize $\sum_{n=1}^M w_n [Y_n - F(X_n)]^2$, $w_1 \neq 0$, modify the PHI and Y arrays as follows:

$$\text{PHI} = \begin{bmatrix} \sqrt{w_1} \text{PHI}(1,1) & \sqrt{w_1} \text{PHI}(1,2) & \dots & \sqrt{w_1} \text{PHI}(1,N) \\ \sqrt{w_2} \text{PHI}(2,1) & \dots & \dots & \dots \\ \vdots & & & \\ \sqrt{w_M} \text{PHI}(M,1) & \dots & \dots & \sqrt{w_M} \text{PHI}(M,N) \end{bmatrix}$$

$$Y = \begin{bmatrix} \sqrt{w_1} Y(1) \\ \sqrt{w_2} Y(2) \\ \sqrt{w_3} Y(3) \\ \vdots \\ \sqrt{w_M} Y(M) \end{bmatrix}$$

Sample Problem

Find the second degree polynomial $F = A_3 x^2 + A_2 x + A_1$, which best fits the following data in the least squares sense, where $M = 9$, $N = 3$, $NT = 1$.

X -4., -3., -2., -1., 0., 1., 2., 3., 4.
Y -2., -3., -6., -7., -6., -3., 2., 9., 18.

Solution is $F = X^2 + 2X - 6$.

Sample Solution

```

NEW
NEW FILE NAME--EXAMPLE
READY

10 COMMON PHI(9,3),X(9),A(3),RW(27)
20 COMMON AM(3,3),Y(9),YA(9),NS(1)
30 DATA M,N,NT,NS/9,3,1,9/
40 INPUT,(X(I),I=1,M)
50 INPUT,(Y(I),I=1,M)
60 CALL PH11(M,N)
70 CALL LSQMM(PHI,Y,A,RW,M,N,NT,NS,AM,9,3)
80 DO 40 I=1,M
90 YA(I)=0.0
100 DO 30 J=1,N
110 50 YA(I)=YA(I)+A(J)*PHI(I,J)
120 40 CONTINUE
130 PRINT 100
140 100 FORMAT("      X      F(X)      Y-F(X)      A(N)
150 &      ")
170 DO 50 I=1,N
180 50 PRINT 60,X(I),YA(I),RW(I),A(I)
190 60 FORMAT(4E13.4)
200 K=N+1
210 DO 70 I=K,M
220 70 PRINT 80,X(I),YA(I),RW(I)
230 80 FORMAT(3E13.4)
240 STOP
250 END

260 SUBROUTINE PH11(M,N)
270 COMMON PHI(9,3),X(9)
280 DO 10 I=1,M
290 10 PHI(I,1)=1.0
300 IF(N-2) 40,15,15
310 15 DO 30 I=1,M
320 DO 20 J=2,N
330 20 PHI(I,J)=X(I)**(J-1)
340 30 CONTINUE
350 40 RETURN
360 END

```

RUN

EXAMPLE

X -4., -3., -2., -1., 0., 1., 2., 3., 4.
Y -2., -3., -6., -7., -6., -3., 2., 9., 18.

X	F(X)	Y-F(X)	A(N)
-0.6000E+01	-0.6000E+01	0.	-0.6000E+01
-0.2000E+01	-0.2000E+01	0.	0.2000E+01
-0.2000E+01	-0.6000E+01	0.	0.1000E+01
-0.1000E+01	-0.7000E+01	0.	
0.	-0.6000E+01	0.	
0.1000E+01	-0.3000E+01	0.	
0.2000E+01	0.2000E+01	0.	
0.3000E+01	0.9000E+01	0.	
0.4000E+01	0.1800E+02	0.	

APPENDIX B

INPUT-OUTPUT DESCRIPTION

INPUT-OUTPUT DESCRIPTION

PROGRAM NAME - SPIN-73

CODING DATE - July 1973

PURPOSE - Predict the aerodynamic coefficients of spin stabilized projectiles at Mach numbers for 0.0 to 5.0.

Inputs to the program are the projectile physical dimensions, projectile mass properties, gun bore diameter and twist, and the local air temperature.

INPUTS

Card No. 1 (See Note D)

<u>IBM CARD COL</u>	<u>VARIABLE</u>	
1 - 7	VL	Projectile length - calibers
8 - 14	VN	Ogive length - calibers
15 - 21	VB	Boattail length - calibers
22 - 28	VCG	Center of gravity - calibers for nose
29 - 35	DM	Diameter Me'Plat - calibers
36 - 42	BD ^B	Rotating band diameter - calibers
43 - 49	OR ^B	Ogive radius - calibers
50 - 56	BOOM	Boom length - calibers
57 - 80	NTITLE	Descriptor

Card No. 2 (See Note C)

1 - 7	DIA	Projectile diameter - inches
8 - 14	AX	Axial inertia - inches lb-in ²
15 - 21	TR	Transverse inertia - inches lb-in ²
22 - 28	WGT	Projectile weight - lbs.
29 - 35	TWIST	Gun twist - cal/turn
36 - 42	TFMP	Air temperature - °F
43 - 49	DGUN ^B	Gun bore diameter - inches
50 - 56	NAUTO ^A	0 Uses input dimensions 1 Automatic dimensions

A

BD set equal to 1.02 calibers
DM set equal to 0.12 calibers
OR set equal to 2 (-VN²) (secant ogive)

B

If input as zero (0.0) these inputs are changed
BD set equal to 1.00 calibers
OR set equal to secant ogive
DGUN set equal to DIA

C

If aero estimates are only requirement
this card should be left blank.

D

Repeat cards 1 and 2 to stack cases

OUTPUTS

- Line 1 - Organization designation
- Line 2 - Description of item being estimated
- Line 3 - Title line - projectile dimensions
- Line 4 - Projectile dimensions
- Line 5 - Title line - projectile physical properties, gun properties
air temperature and density
- Line 6 - Projectile physical properties, gun properties, air temperature
and density
- Line 7 - 'Aerodynamic Coefficients'
- Line 8 - Title line - Mach No., etc.
- Line 9 - Cxo - Zero yaw axial force coefficient
CX2 - Yaw axial force coefficient per $\sin^2 \alpha$
CNA - Normal force coefficient derivative per $\sin \alpha$
CMA - Pitching moment coefficient derivative per $\sin \alpha$
CPN - Normal force center of pressure - calibers for nose
CYP - Magnus force coefficient derivative per $\sin \alpha$
CNPA - Zero yaw Magnus moment coefficient derivative per $\sin \alpha$
CNPA3 - Cubic Magnus moment coefficient derivative per $\sin^3 \alpha$
CNPA5 - Quintic Magnus moment coefficient derivative per $\sin^5 \alpha$
CPF1 - Center of pressure of Magnus force at 1° yaw or less
calibers from nose
CPF5 - Center of pressure of Magnus force at 5° yaw, calibers
from nose
CNPA-5 - 5° - Secant slope of Magnus moment coefficient
derivative (at 5° yaw) per $\sin \alpha$
Cmq - Damping moment coefficient
Clp - Spin deceleration coefficient
- Line 10 - 'Stability Analysis'
- GYRO Gyroscopic stability factor
- SBAR Dynamic stability factor at 1° yaw
- RECIP Dynamic reciprocal factor at 1° yaw
- SBAR5 Dynamic stability factor at 5° yaw
- RECIP5 Dynamic reciprocal factor at 5° yaw
- SPIN Spin rate, radians/second
- W1 Nutation frequency, radians/second
- W2 Precession frequency, radians/second
- L1 Nutation damping factor per foot @ 1° yaw
- L2 Precession damping factor per foot @ 1° yaw
- L1-5 Nutation damping factor per foot @ 5° yaw
- L2-5 Precession damping factor per foot @ 5° yaw
- DELT Integration time step, seconds (20 per nutation)
- DISP Dispersion factor per 5° first max yaw, mils

APPENDIX C
PROGRAM LISTING
SPIN-73

DATE	TIME	GE-400 SERIES	CONTRAST	ASA	INSTR.	PAGE	F	X	SPIN	0508
51		C								
52		C								
53		C								
54		C								
55		C								
56		C								
57		C								
58		C								
59		C								
60		C								
61		C								
62		C								
63		C								
64		C								
65		C								
66		C								
67		C								
68		C								
69		C								

1001 FORMAT(6F7.0,6A4)
1002 FORMAT(7F7.0,20X,10I1)

SPIN1430
SPIN1440
SPIN1450

Best Available Copy

06/28/73

SPIN-73-

THE GE-400 SERIES - CONT'D: ASA (MIPC)

PAGE # 4 SPIN 0508

```

70 1999 FORMAT(1H1)
71 2000 FORMAT(4X,2M OF BURLINGTON VERMONT /5X,644//)
72 2001 FORMAT(1X,5HTOTAL,1X,5HNOSE /8X,9HBOAT TAIL,9X,3HNOSE /10X,7HMEPLA
   *T /9X,5HBRAND /1X,5HNOSE /1X,5HROOM /4X,3HLENGHTM /1X,9HCFW
   *NOSE) /1X,9HDIAMETER /1X,6HRAADIUS,10X,6HLENGTM
73 2002 FORMAT(1X,1F10.3,5X)
74 2003 FORMAT(// 3X,9HDIAMETER /9X,3H1X /12X,3H1Y /10X,7HFLIGHT /7X,9HCU
   *R TWIST /4X,13HACTUAL TWIST /4X,9HGUN-BORE /5X,13HTEMPERATURE /4X,11
   *HAIR DENSITY /4X,7HINCHES /1X,2HAX,9HLR-14-50 /9X,5HMS,3X,2HAX,9
   *MCAL/TUHA /1X,7HINCHES /9X,5HCEG-F,7X,11HSLUGS/10.3
75 2004 FORMAT(1X,1F10.3,5X)
76 2005 FORMAT( //4X,26H AERODYNAMIC COEFFICIENTS //5X,5HMAC,5X,3HCY
   * /4X,3HXC2,6X,3HMAC,4X,3HMAC,6X,3HCPN,5X,5HGYA /4X,5HMACPA /4X,5H
   *LP)
77 2006 FORMAT(1X,1F10.3)
78 2007 FORMAT( //5X,20H STABILITY ANALYSIS //5X,5HMACF /4X,5HGYRO /4X,
   *5HSHAR /4X,5HRECIP,3X,7HSHAR*5 /2X,7HRECIP*5,3X,5HCUIN /5X,3Hw1 /6
   *X,3Hw2 /4X,3H1 /6X,3H2 /5X,5H1*5 /4X,5H2*5 /4X,4HDEL1,5X,
   *4HDEL2)
79 2008 FORMAT(1X,6F9.3,9.3,2F9.2,4F9.6,4F9.4,7F9.3)
80 2010 FORMAT(1X,2F9.3
81 3999 FORMAT(10F7.3)
82 1H=6
83 1R=50
84 1R=50
85 CALL EOSTST(1R,1)
86 IF(1.EQ.2) STOP
87 READ(1R,1002) DIA,AX,TR,WT,TWIST,TEMP,NGUN,NAUTO,NAFRO,NSAUL,NMOL,
   *NOLICK,NGRAPH
88 IF(NAUTO-1) 3,2,2
89 2 RD=1.02
90 DM=12
91 OR=VA*VN*2
92 RMC=.002374*(-4.784*(TEMP-59.))-.01092*(TEMP-59.)*.000001
93 ASO=.49.04*SQRT(459.6*(TEMP)
94 IF(DGUN) 4,4,5
95 4 IF(DIA) 155,155,45
96 45 DGUN=DIA
97 5 TT=(1./TWIST*DIA/NGUN)**2
98 TT=1.0/TWIST
99 155 CONTINUE
100 IF(RD) 6,6,7
101 6 RD=1.
102 7 IF(OR) 8,9
103 8 OR=VA*VN*2.
104 9 CONTINUE
105 WRITE(1W,1999)
106 WRITE(1W,2000) (NTITLE(1),I=1,6)
107 WRITE(1W,2001)
108 WRITE(1W,2002) VI,VN,VB,VCG,DH,8D,OR,BOOM
109 WRITE(1W,2003)
110 WRITE(1W,2004) DIA,AX,TR,WT,TWIST,TEMP,NGUN,DIA,NGUN,TEMP,RMD
111 C
      SETUP OF CONSTANTS

```

SPIN1680

Best Available Copy

06/26/73

SPIN-73

THE GE-400 SERIES - FORTRAN ASA (MTPS)

PAGE # 5

SPIN 0500

```

C      SETUP OF CONSTANTS
112  ZRC=0.0
113  ZPTV=0.25
114  ZPV=0.5
115  ONE=1.0
116  TWC=2.0
117  POR=4.0
118  POP=4.0
119  VIV=5.0
120  SEAG=5.51
121  TLV=12.0
122  GRAVYE=32.174
123  DD=DIA/DIA
124  FD=DIA*VIV
125  XZ=AY*AX
126  D=DIA/TLV
127  AR=D*0.7854
128  AXL=AX/(TLV*TLV)
129  TRL=TR/(TLV*TLV)
130  A=AXI/GRAVY
131  B=TRL/GRAVY
132  VVL=VL*VL
133  TK=(KG*DD)/AX
134  RK=(LG*DD)/TR
135  FACT=RO*GRAVY*AR/(POR*HGT)
136  DKH=((VVL/VIV)-VL)*5.73
137  CVL=VL
138  CXCL=VL*VM-VB-L*5
139  CVA=VN-2.5
140  CVR=VR
141  CBL=BD-1.02
142  CDP=(DM-12)*2
143  CRI=VA*VN/0.4
144  CCG=VCR-3.0
145  CLL=VL-5.0
146  DO=500/21.17
147  AXIAL FORCE
148  IF(VRX.LT.0.0) VRX=0.0
149  VN=VM
150  CXCLL=CXCL
151  DXET=0.0
152  DXA=0.0
153  DXCL=0.0
154  VRX=0.45
155  VBX=0.45
156  IF(VB-1.0) 307,307,308
157  DXET=(VB-0.65)*XA10(J)
158  GO TO 302
159  308 DXBT=XA10(J)*0.35*(VR-1.0)*XA10(J)*0.3333
160  302 IF(VA-LE.3.0) GO TO 304
161  VNX=3.0
162  IF(VA.GT.3.48) GO TO 309
163

```

SPIN2090

C

Best Available Copy

```

154 DXN=(V-3.0)*X13(J)
155 GO TO 304
156 309 IF(CVA-CT-3.97) GO TO 310
157 DXN=0.48*X13(J)*(VN-3.48)*X14(J)
158 GO TO 304
159 310 DXN=0.48*X13(J)*0.49*X14(J)*(VN-3.97)*X15(J)
160 304 IF(CXCL-1.5) 306,306,305
161 DXCL=(CXCL-1.5)*0.010
162 CXCL=(CXCL-1.5)*0.010
163 306 CONTINUE
164 CX0=X1(J)*X17(J)*(VNX-2.5)*X1(J)*(VNX-2.5)*X14(J)*(VNX-2.5)*
165 13*X15(J)*CXCL(X16(J)*CXCL(X17(J)*X17(J)*X17(J)*X17(J)*X17(J)*
166 2*X1A(J)*CRAT*X19(J)*CRAT=2
167 3-X11(J)*CHD*X12(J)*CDM=(ROCM/1.36)*2*0.01
168 4-EXHT-DXN-DXCL
169 C COMPLETION OF CONSTANTS FOR CA AND CMA
170 VNX=VH
171 DXN=0.0
172 IF(CVA-3.0) 11,13,10
173 10 VNX=3.0
174 DXN=V-3.0
175 GO TO 12
176 11 CONTINUE
177 VNX=VH
178 12 IF(VR-1.0) 14,14,13
179 13 VNX=1.0
180 VBP=VR*0.5
181 VPP=VR*0.5
182 GO TO 25
183 14 CONTINUE
184 IF(J.GF.5) GO TO 20
185 VBP=VH
186 VRP=VR*0.8
187 GO TO 25
188 20 CONTINUE
189 VBP=VR*1.5
190 VRP=VR
191 25 CONTINUE
192 CVA=VNX-2.47
193 CDP=DP-0.17
194 CRD=RD-1.04
195 CRD=RD-1.04
196 CCRT=VN*VH/OR-0.44
197 VRT=CVL/4.7
198 CNA8=X1(J)*X17(J)*CVNN*X13(J)*CXCL(X14(J)*CCRT*X15(J)*CVNN*CVNN
199 CNET=VRNP*X17(J)*VRX*CVNN*X18(J)*VHX*CXCL(X19(J)
200 IF(CART,GT,0.0) CNPT=0.0
201 CNA7=CNA8*CNPT
202 AMCSQ=CNAR*(VC1(J)*XC2(J)*CVNA*X13(J)*CVNN*CVNN*X14(J)*CVNN
203 1*CVNA*CVNN*X15(J)*CXCL(X16(J)*CXCL(X17(J)*CXCL(X18(J)*CXCL(X19(J)*
204 2*XC8(J)*CCRT*YC9(J)*CCRT*CCRT*XC10(J)*CDMM
205 3*XC11(J)*CCRT*CVNN*DXN*XC17(J)
206 AMCMT=VRT*(VHNP*VC12(J)*VHX*CVNN*XC13(J)*VHX*CXCL(X14(J)

```

Best Available Copy

15/20/73

SPIN 9508

THE GE-400 S/RFC - (M)UAW AS4 (M)PLC

PAGE 7

SPIN 9508

```

213 *VHVE=CHT*XC1*(J)*VHX*CCRT*CVN*XC16(J))
214 IF (APN*BT*G*E*O) CNAT=CNAR
215 IF (A*O*BT*G*E*O) AMO*BT=0.0
216 CPN=(AMOPSO*APOMHT)/CNAT
217 CHAT=(UG*CON)*CNA
218 CY2*BT(J)*X2*BT(J)*CXCL*XD3(J)*CRAT*XD4(J)*CVR=CNA*
219 COM*BT(J)*CVA
220 CYF*BT(J)*CV
221 CYFAC*CV*0.1*CVN
222 COM*BT(J)*CPE AND CNPA AT A=1.0
223 DCFE=0.0
224 IF (VLE*E*6*O) GO TO 28
225 DCFE*(VLE*6*O)*E5(J)
226 28 CONTINUE
227 CNFA=CVA*(XF2(J)*0.55*CYCL*0.8*CVN)
228 C*1.0*CVL/4.7*CVN
229 CPE=C*PAH/CVA
230 CPE*BT(J)*CPE
231 CNIA=IV(G*CFE)*CVA
232 COM*BT(J)*CPE AND CNPA AT A=2.0
233 CNFA=CVA*(XF3(J)*0.55*CXCL*0.8*CVN)
234 C*1.0*CVL/4.7*CVN
235 CPE=C*PAH/CVA
236 CPE*BT(J)*CPE
237 CNFA2=(VGO*CFE)*CVA
238 COM*BT(J)*CPE AND CNPA AT A=5.0
239 CNFA=CVA*(XF4(J)*0.55*CXCL*0.8*CVN)
240 C*1.0*CVL/4.7*CVN
241 CPE=C*PAH/CVA
242 CPE*BT(J)*CPE
243 CNFA5=(VGO*CFE)*CVA
244 COM*BT(J)*CPE
245 DCFE=0.0
246 IF (VLE*E*6*O) GO TO 30
247 DCFE*(VLE*6*O)*E9(J)
248 30 CONTINUE
249 CM*BT(J)*XF2(J)*CLL*XF3(J)*CLL*XF4(J)*CCG*XF5(J)*CCG*CLL*XF6(J)
250 *J)*CCG*CLL*CLL*XF7(J)*CCG*CVB*YFA(J)*CVB
251 CM*BT(J)*XF2(J)*CLL*XF3(J)*CLL*XF4(J)*CCG*CVB*YFA(J)*CVB
252 CM*BT(J)*XF2(J)*CLL*XF3(J)*CLL*XF4(J)*CCG*CVB*YFA(J)*CVB
253 COM*BT(J)*CLP
254 CLP=VCL(J)*VLE/SPNG
255 554 STABILITY CALCULATIONS
256 IF (DIA155*555*554
257 STAB(J)=152.4*XY*TT/(1.0*RH0*F*CHA)
258 ROT1=CNAT*CX0*(BK*7PV*CHD)*(TK*ZPV*CLP)
259 ROT1=CNAT*CX0*(BK*7PV*CHD)*(TK*ZPV*CLP)
260 SHAR1=TOP1/HUT1
261 RECPS=ONE/(SHAR1*(TWO-SBAR1))
262 TOS=TWO*(CNAT*CX0*TK*ZPV*CNPA5)
263 SHAR=TOP5/ROT1
264 RECPS=ONE/(SHAR5*(TWO-SBAR5))

```

SPIN3010

SPIN3030

SPIN3060

SPIN3090

SPIN3120

SPIN3180

SPIN3200

SPIN3210

SPIN3220

SPIN3230

SPIN3240

SPIN3270

SPIN3290

SPIN3300

SPIN3310

16/28/73

SPIN-74

TWE GE-400 SERIES - (M)TAN ASA (MTPS)

PAGE 4

SPIN 0508

244 IF (STAR(J)=1.01) 50.55.55
 245 SS=ONE-(ONE/STAR(J))
 246 SIGMA((1555*74V
 247 VEL=CHACH(J)*ASSO
 248 PC(J)=6.283*VEL/D*Q(4/DGUR
 249 A1(J)=PC(J)*AY/(T*W*TH))*(ONE-SIGMA(J))
 250 A2(J)=PC(J)*AY/(T*W*TH))*(ONE-SIGMA(J))
 251 D155(J)=((CNAT-CYNO*TH*(J))-21.11)*3.635)/(CMA*RG*DI*VEL)
 252 TAU*CNK/SIGMA(J)
 253 A1*EFFECT*((CNAT)*(ONE-TAU))*(RK/THO)*(ONE-TAU)*CMO*TK*TAU*CMPA)
 254 A2*EFFECT*((CNAT)*(ONE-TAU))*(RK/THO)*(ONE-TAU)*CMO*TK*TAU*CMPA)
 255 H*EFFECT*((CNAT)*(ONE-TAU))*(RK/THO)*(ONE-TAU)*CMO*TK*TAU*CMPAAS)
 256 A2*EFFECT*((CNAT)*(ONE-TAU))*(RK/THO)*(ONE-TAU)*CMO*TK*TAU*CMPAAS)
 257 A1(J)=A1
 258 A2(J)=A2
 259 RL(J)=TH
 260 RL2(J)=H2
 261 DELT(J)=6.28/(1(J)*20.0)
 262 GO TO 56
 555 STAR(J)=740
 263 STAR(J)=740
 264 STAR(J)=740
 265 HELPS=40
 266 RECPS=740
 267 SRAR=740
 56 CONTINUE
 268 SD1(J)=SPAR
 269 RI(J)=HECP1
 270 SD5(J)=SRAR5
 271 RS1(J)=HECP5
 272 X*AG2*CNPAAS-C*PA*0.1
 273 CNPASE*XMAG2-9.0*XMAG1/0.0072
 274 CNPASE*XMAG1-CAPA5*.00011/0.01
 556 WRITE(14,2006)(CHACH(J),CYO,CX2,CNAT,CHA,CPN,CYPA,CNPA,CNPA3,CNPA5,
 1 CCF,COF15,CNPAAS,CMO,CLP
 500 CONTINUE
 275 IF (DIAT(1,1)=55A
 276 WRITE(A,20A7)
 277 DO 501 J=1,7
 278 IF (STAR(J)=1.001) 57.58.5A
 279 WRITE(A,2010) CHACH(J),STAR(J)
 280 GO TO 59
 58 WRITE(14,2008) CHACH(J),STAR(J),SD1(J),RI(J),SD5(J),RS1(J),P(J),
 1 W1(J),W2(J),AL1(J),AL2(J),BL1(J),BL2(J),DELT(J),DISP(J)
 59 CONTINUE
 501 CONTINUE
 281 GO TO 1
 282
 283
 284
 285
 286
 287
 288
 289
 290
 291
 292
 293
 294
 295
 296
 297
 298
 299
 300
 301
 302
 303
 304
 305
 306
 307
 308
 309
 310
 311
 312
 313
 314
 315
 316
 317
 318
 319
 320
 321
 322
 323
 324
 325
 326
 327
 328
 329
 330
 331
 332
 333
 334
 335
 336
 337
 338
 339
 340
 341
 342
 343
 344
 345
 346
 347
 348
 349
 350
 351
 352
 353
 354
 355
 356
 357
 358
 359
 360
 361
 362
 363
 364
 365
 366
 367
 368
 369
 370
 371
 372
 373
 374
 375
 376
 377
 378
 379
 380
 381
 382
 383
 384
 385
 386
 387
 388
 389
 390
 391
 392
 393
 394
 395
 396
 397
 398
 399
 400
 401
 402
 403
 404
 405
 406
 407
 408
 409
 410
 411
 412
 413
 414
 415
 416
 417
 418
 419
 420
 421
 422
 423
 424
 425
 426
 427
 428
 429
 430
 431
 432
 433
 434
 435
 436
 437
 438
 439
 440
 441
 442
 443
 444
 445
 446
 447
 448
 449
 450
 451
 452
 453
 454
 455
 456
 457
 458
 459
 460
 461
 462
 463
 464
 465
 466
 467
 468
 469
 470
 471
 472
 473
 474
 475
 476
 477
 478
 479
 480
 481
 482
 483
 484
 485
 486
 487
 488
 489
 490
 491
 492
 493
 494
 495
 496
 497
 498
 499
 500
 501
 502
 503
 504
 505
 506
 507
 508
 509
 510
 511
 512
 513
 514
 515
 516
 517
 518
 519
 520
 521
 522
 523
 524
 525
 526
 527
 528
 529
 530
 531
 532
 533
 534
 535
 536
 537
 538
 539
 540
 541
 542
 543
 544
 545
 546
 547
 548
 549
 550
 551
 552
 553
 554
 555
 556
 557
 558
 559
 560
 561
 562
 563
 564
 565
 566
 567
 568
 569
 570
 571
 572
 573
 574
 575
 576
 577
 578
 579
 580
 581
 582
 583
 584
 585
 586
 587
 588
 589
 590
 591
 592
 593
 594
 595
 596
 597
 598
 599
 600
 601
 602
 603
 604
 605
 606
 607
 608
 609
 610
 611
 612
 613
 614
 615
 616
 617
 618
 619
 620
 621
 622
 623
 624
 625
 626
 627
 628
 629
 630
 631
 632
 633
 634
 635
 636
 637
 638
 639
 640
 641
 642
 643
 644
 645
 646
 647
 648
 649
 650
 651
 652
 653
 654
 655
 656
 657
 658
 659
 660
 661
 662
 663
 664
 665
 666
 667
 668
 669
 670
 671
 672
 673
 674
 675
 676
 677
 678
 679
 680
 681
 682
 683
 684
 685
 686
 687
 688
 689
 690
 691
 692
 693
 694
 695
 696
 697
 698
 699
 700
 701
 702
 703
 704
 705
 706
 707
 708
 709
 710
 711
 712
 713
 714
 715
 716
 717
 718
 719
 720
 721
 722
 723
 724
 725
 726
 727
 728
 729
 730
 731
 732
 733
 734
 735
 736
 737
 738
 739
 740
 741
 742
 743
 744
 745
 746
 747
 748
 749
 750
 751
 752
 753
 754
 755
 756
 757
 758
 759
 760
 761
 762
 763
 764
 765
 766
 767
 768
 769
 770
 771
 772
 773
 774
 775
 776
 777
 778
 779
 780
 781
 782
 783
 784
 785
 786
 787
 788
 789
 790
 791
 792
 793
 794
 795
 796
 797
 798
 799
 800
 801
 802
 803
 804
 805
 806
 807
 808
 809
 810
 811
 812
 813
 814
 815
 816
 817
 818
 819
 820
 821
 822
 823
 824
 825
 826
 827
 828
 829
 830
 831
 832
 833
 834
 835
 836
 837
 838
 839
 840
 841
 842
 843
 844
 845
 846
 847
 848
 849
 850
 851
 852
 853
 854
 855
 856
 857
 858
 859
 860
 861
 862
 863
 864
 865
 866
 867
 868
 869
 870
 871
 872
 873
 874
 875
 876
 877
 878
 879
 880
 881
 882
 883
 884
 885
 886
 887
 888
 889
 890
 891
 892
 893
 894
 895
 896
 897
 898
 899
 900
 901
 902
 903
 904
 905
 906
 907
 908
 909
 910
 911
 912
 913
 914
 915
 916
 917
 918
 919
 920
 921
 922
 923
 924
 925
 926
 927
 928
 929
 930
 931
 932
 933
 934
 935
 936
 937
 938
 939
 940
 941
 942
 943
 944
 945
 946
 947
 948
 949
 950
 951
 952
 953
 954
 955
 956
 957
 958
 959
 960
 961
 962
 963
 964
 965
 966
 967
 968
 969
 970
 971
 972
 973
 974
 975
 976
 977
 978
 979
 980
 981
 982
 983
 984
 985
 986
 987
 988
 989
 990
 991
 992
 993
 994
 995
 996
 997
 998
 999
 1000

Best Available Copy

DISTRIBUTION LIST

	Copy No.
Commander	
U. S. Army Material Command	
ATTN: AMCRD-TP, Mr. J. Hughes	1
AMCRD- Dr. J. V. R. Kaufman	2
5001 Eisenhower Ave.	
Alexandria, VA 22304	
 Commander	
Ballistic Research Laboratories	
ATTN: Dr. C. Murphey	3
Mr. L. MacAllister	4
Mr. R. McCoy	5
Technical Library	6
Aberdeen Proving Grounds, MD 21005	
 Commander	
U. S. Army Armaments Command	
ATTN: Mr. Brinkman	7
Dr. E. Haug	8
Technical Library	9
Rock Island, IL 61202	
 Commander	
U. S. Army Missile Command	
ATTN: Mr. R. A. Deep	10
Technical Library	11
Huntsville, AL 35809	
 Commander	
Harry Diamond Laboratory	
ATTN: Technical Library	12
Washington, DC 20438	
 Commander	
U. S. Army Material Command	
ATTN: Deputy for Laboratories, AMCDL	13
Chief of Laboratory Operations, Mr. H. Kline, AMCDL	14
5001 Eisenhower Ave.	
Alexandria, VA 22304	
 Director	
U. S. Army Ballistic Missile Defense Agency	15
1320 Wilson Blvd.	
Arlington, VA 22209	
 Director	
U. S. Army Advanced Material Concepts Agency	16
2461 Eisenhower Ave.	
Alexandria, VA 22314	

Commander U. S. Army Edgewood Arsenal ATTN: Technical Library Edgewood Arsenal, MD 21010	17
Commander U. S. Army Frankford Arsenal ATTN: Mr. S. Hershman Mr. C. Bateman Technical Library Philadelphia, PA 19137	18 19 20
Director Advanced Research Projects Agency Department of Defense Washington, DC 20301	21
Commander U. S. Naval Weapons Center ATTN: Dr. W. Haseltine Technical Library China Lake, CA 93555	22 23
Commander U. S. Naval Weapons Laboratory ATTN: Dr. T. Clare Mr. R. Whalen Dr. W. Kemper Mr. P. Daniels Mr. G. R. Bolick Technical Library Dahlgren, VA 22448	24 25 26 27 28 29
Commander U. S. Naval Ordnance Laboratory ATTN: Mr. S. Hastings Technical Library White Oak, Silver Spring, MD 20910	30 31
Commander Air Force Armament Laboratory ATTN: Mr. F. Burgess Mr. C. Butler Technical Library Eglin Air Force Base, FL 32542	32 33 34
Commander Air Force Weapons Laboratory ATTN: Technical Information Section Kirtland Air Force Base, NM 87117	35

Commander Defense Documentation Center Cameron Station Alexandria, VA 22314	36-37
Commander Air Proving Ground Center (PGTRI) ATTN: Technical Library	38
Mr. F. Burgess	39
Mr. E. Sears	40
Eglin Air Force Base, FL 32542	
Commander U. S. Naval Weapons Laboratory ATTN: Mr. C. Wingo	41
Dr. W. Kemper	42
Mr. J. Roman	43
Mr. Moore	44
Dahlgren, VA 22314	
General Electric Company ATTN: Armament Systems Department Burlington, VT 05401	45-50
Commander Picatinny Arsenal ATTN: STIB	
Dr. E. Sharkoff	51-55
Mr. S. Kravitz	56
Mr. V. Lindner	57
Mr. S. Wasserman	58
Mr. J. Gregorits	59
Mr. J. Dubin	60
Mr. A. LoPresti	61
Mr. A. Loeb	62
Mr. D. Lertz	63-72
Mr. R. Kline	73-77
Dover, NJ 07801	

UNCLASSIFIED

Security Classification

DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author)		2a. REPORT SECURITY CLASSIFICATION	
Armament Systems Department General Electric Co. Burlington, VI 05401		UNCLASSIFIED	
3. REPORT TITLE		2b. GROUP	
Spin-73 An Updated Version of the Spinner Computer Program			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)			
5. AUTHOR(S) (First name, middle initial, last name)			
Robert H. Whyte			
6. REPORT DATE	7a. TOTAL NO OF PAGES	7b. NO OF REFS	
NOVEMBER 1973	89	75	
8a. CONTRACT OR GRANT NO	9a. ORIGINATOR'S REPORT NUMBER(S)		
DAAA21-73-C-0033	Technical Report 4588		
b. PROJECT NO	9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)		
AMCMS Code No. 554C.12.62000			
c.			
d.			
10. DISTRIBUTION STATEMENT			
Distribution limited to U.S. Government agencies only (test and evaluation, November 1973). Other requests for this document must be referred to Picatinny Arsenal, Dover, N.J.. ATTN: SAPPA-TS-T-5.			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY	
		Feltman Research Laboratory Picatinny Arsenal Dover, N.J. 07801	
13. ABSTRACT			
<p>The SPINNER computer program has been updated to compute aerodynamic coefficients for a wide variety of spin stabilized projectile shapes. Improvements over the original program are substantial as ogive radius, meplat diameter and rotating band diameter are accounted for instead of assuming mean values. Test cases are shown comparing the 1969 SPINNER, the 1973 SPINNER and experimental data. Input instructions and sample program outputs are given along with the 1973 program listing.</p>			

DD FORM 1473

REPLACES DD FORM 1473, 1 JAN 64, WHICH IS
OBSOLETE FOR ARMY USE

UNCLASSIFIED

Security Classification

UNCLASSIFIED

Security Classification

14	KEY WORDS	LINK A		LINK B		LINK C	
		ROLE	WT	ROLE	WT	ROLE	WT
	Projectile Spin Stability Computer Analysis Drag Pitching Moment Magnus Damping SPINNER						

UNCLASSIFIED

Security Classification



DEPARTMENT OF THE ARMY
US ARMY RESEARCH, DEVELOPMENT AND ENGINEERING COMMAND
ARMAMENT RESEARCH, DEVELOPMENT AND ENGINEERING CENTER
PICATINNY, NEW JERSEY 07806-5000

TECHNICAL REPORT DISTRIBUTION CHANGE

The distribution statement for the below technical paper is to be changed to 1 -
Approved for public release, unlimited.

Title: SPIN-73 an Updated Version of the SPINNER Computer Program
AD Number: AD0915628
Report Date: November 01, 1973

(Signature)

Robert E. Souders
Security Specialist
DPTMS 973-724-4058
DSN 880-4058
US Army Garrison, Picatinny Arsenal

(date)